Chillicothe Road
Bainbridge Twp.
Sec. D.

X 28

FIELD BOOK

302 T

CHILLICOTHE ROAD THRU BAINBRIDGE

Relocation Sta. 146+47.15 to Sta. 197+87.39 1-8

New bench marks 75

Rest of book = slopes, culverts etc.

Spike in Root of 24" Maple
East Side Sta 173+40 1177.84

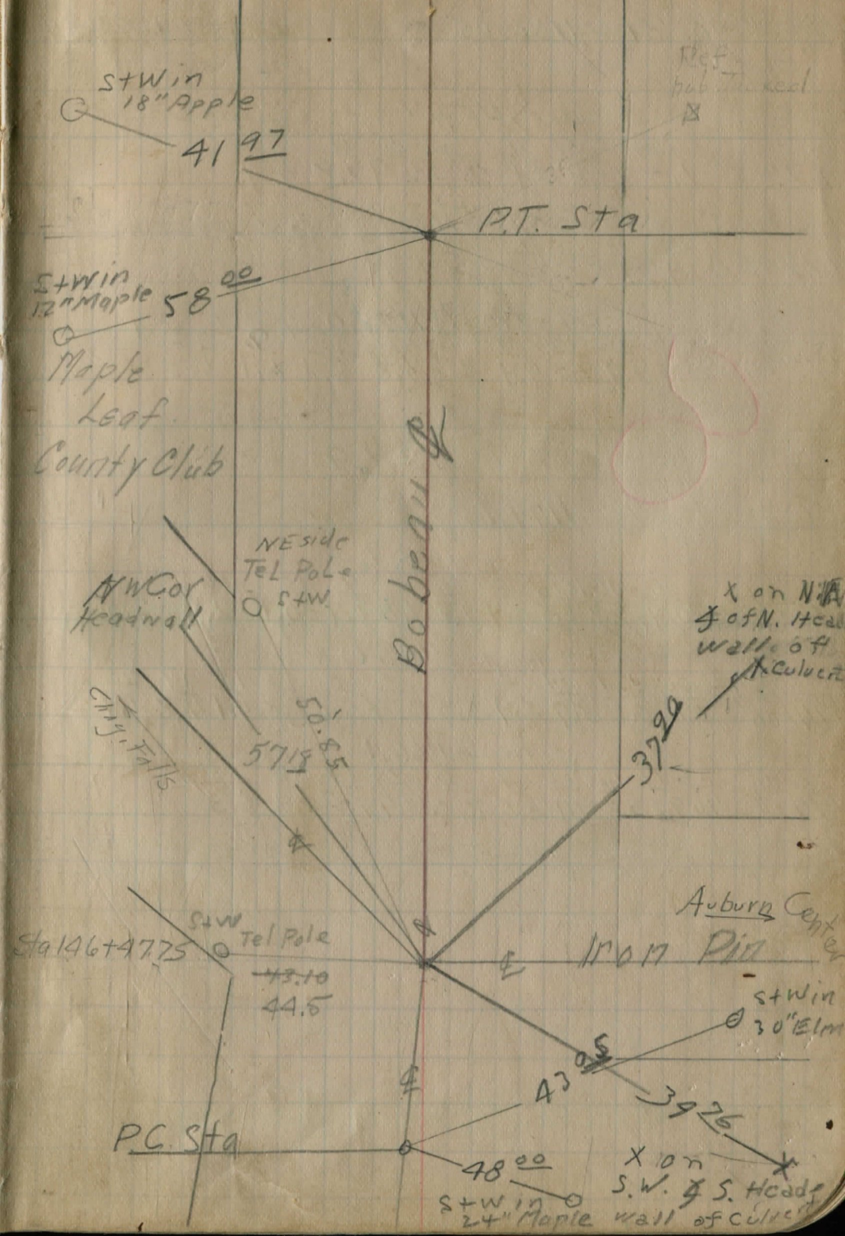
BM Spike in Root 30" Maple
West Side Sta 176+40 1149.34

BM Spike in Root 9" Maple
East Side Sta 178+80 1116.69

BM Sta 185+01 20" Forked Elm
West. Elev 1054.56

BM 187+77 X on NE Cor E Hdwall
Elev 1053.09

Relocation Sta 146+47.75 to Sta 197+87.32



Sta	BS	HI	FS	Elev	BM
1	8.21	1186.05			1177.84

1183.7

172	25	14	11	℄	5	11	25	
	1.5	3.8	3.1	2.3	2.9	1.8	2.7	

Rock 1180.8

172+50	25	18	17	13	℄	12	16	25
	2.4	5.1	5.6	3.3	5.2	5.3	3.2	3.0

Rock 1178.0

173+00	25-30	23	19	9	℄	4	5-7	9	25
	6.3	9.7	9.3	9.1	8.0	7.8	8.1	6.1	5.3

12.69

1.29 1174.65

Rock 1172.7

173+58	25	16-18	14	8	℄	3	4	10	16	25
	-0.4	2.8	2.5	2.4	1.9	1.6	0.7	-0.1	-2.4	-2.5

Rock 1169.1

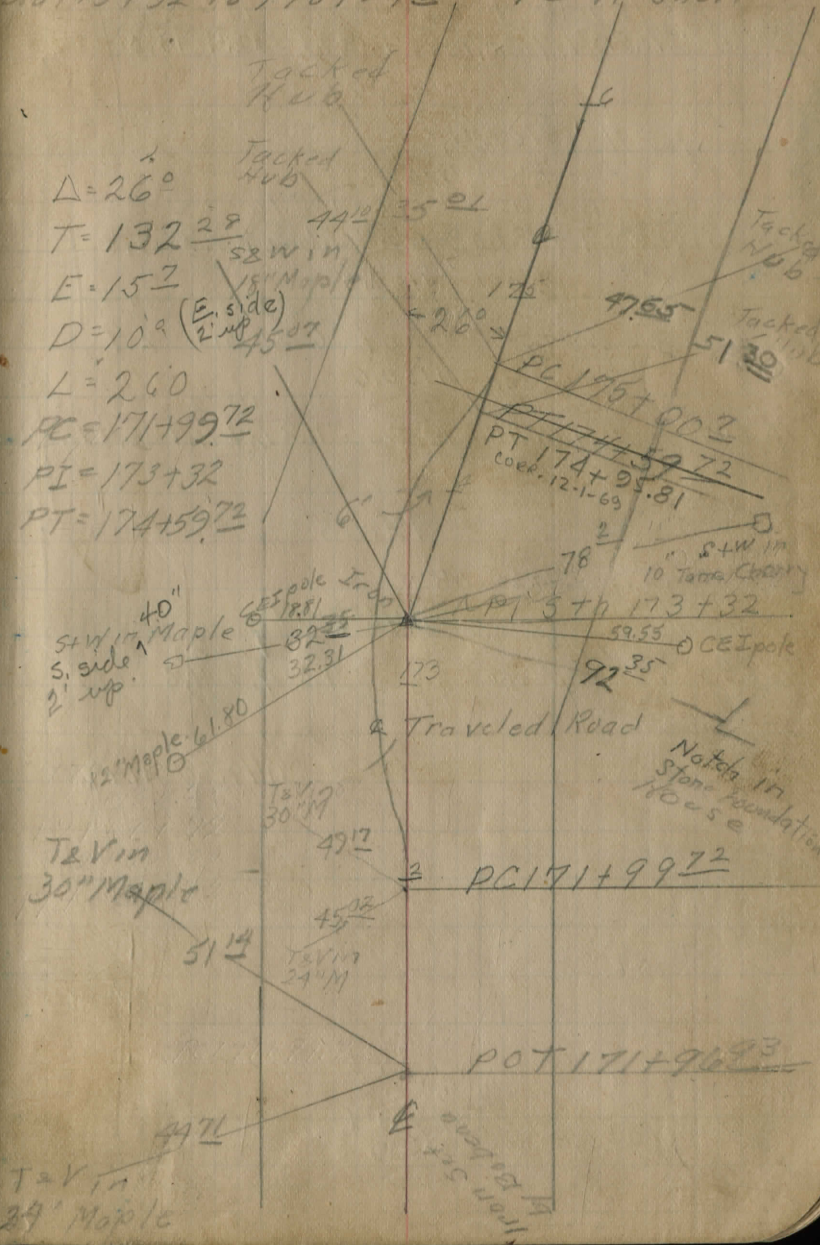
174+00	25	23	20	17-18	14	7	℄	2	8	13	15	19	25
	3.9	4.0	5.6	6.2	5.7	5.4	5.5	5.4	5.6	5.8	5.1	4.8	1.9

Rock 1166.1

174+50	25	22	17	14	15 12	9	℄	10	14	18	25
	7.2	7.6	9.2	9.8	9.1	8.5	8.5	8.7	9.5	9.3	6.3

Mistake in chaining of original survey
Sta 173+32 to 175+24.8 = 4.50 ft short

$\Delta = 26°$
$T = 132.29$
$E = 15.7$ (E. side 2' up)
$D = 10°$
$L = 260$
PC = 171+99.72
PI = 173+32
PT = 174+59.72



1174.65

Rock 1162.1

Sta.										
175+00	25/10.3	18/10.5	15/13.3	10/13.7	7/13.0	℄/12.5	10/12.8	13/13.3	19/12.4	25/10.0

12.81

1.27 1163.11

Rock 1159.5

Sta.											
175+40	25/1.4	18/1.8	13/3.1	10-12/4.5	5/4.0	℄/3.6	5/3.3	12/3.6	16/4.8	22/2.3	25/1.8

Rock 1157.4

Sta.										
175+50	25/3.2	18/3.8	8/4.3	5/6.0	℄/5.7	8/3.7	16/5.6	21/7.0	25/3.1	30-40/2.9

Rock 1150.6

Sta.												
176+00	25/10.4	18/10.4	9/11.3	℄/12.5	3/12.5	12/11.8	17/11.7	21/11.9	25/12.4	28/12.8	37/11.0	40-50/8.5

12.65

0.22 1150.68

1146.9

Sta.							
176+50	25/0.1	18/1.5	℄/3.8	2/4.0	12/4.3	35/4.8	45-55/1.5

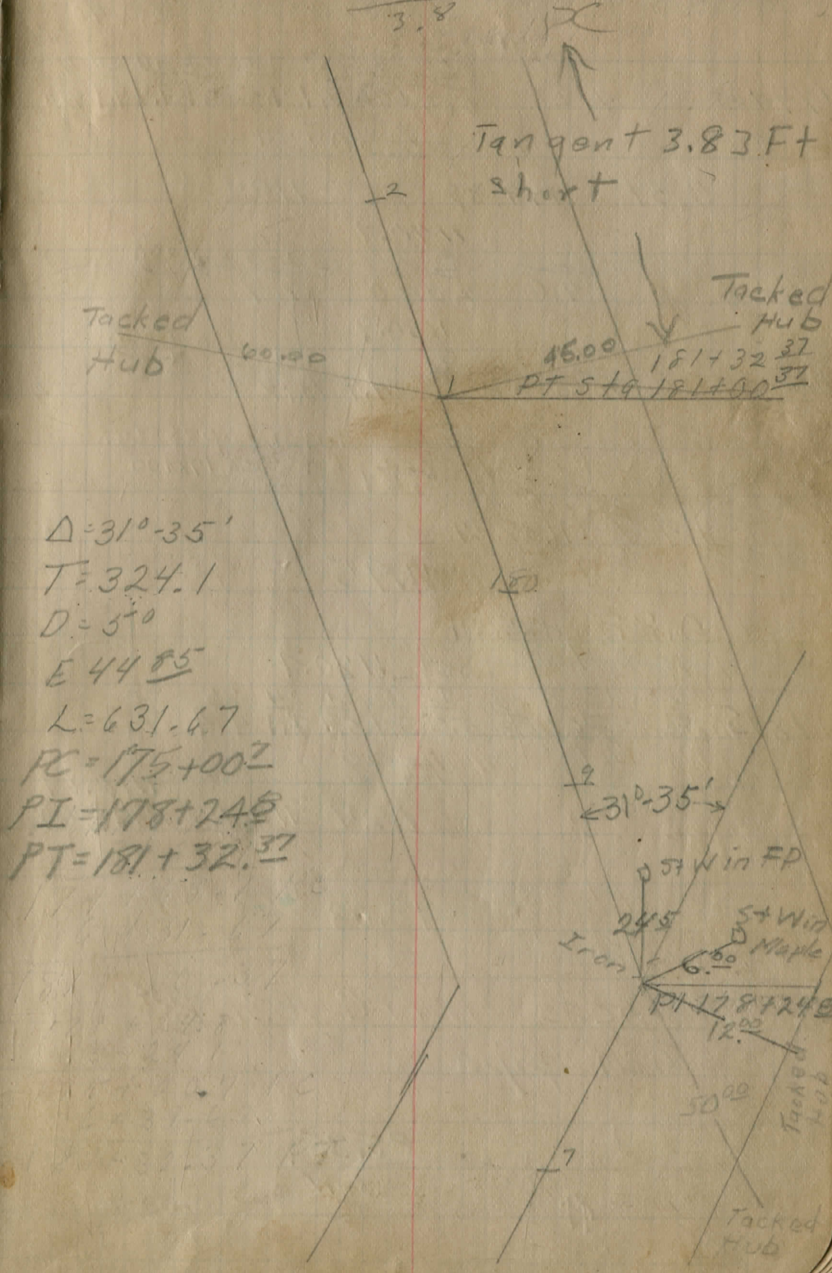
B.M.

1.32 1149.36 1149.36

178+24.8
173+32.8
4+92.8
4+88.3
324.1
1.32.3
4+56.4
3.2

3

1703
138
3.8



Δ=31°-35'
T=324.1
D=5°0
E 44.85
L=631.67
PC=175+00.7
PI=178+24.8
PT=181+32.37

1150.68

Rock 25.40

1145.2

177+00 | 25/4.2 | ℄/5.5 | 3/6.2 | 5/7.1 | 10/7.5 | 14/8.1 | 17/9.7 | 20/9.1 | 40/9.4

6.30 Turn

0.51 1144.89 1144.38

1140.9

177+50 | 25/4.6 | ℄/4.0 | 8/4.0 | 30-50/7.7 Rock

1130.9

178+00 | 25/10.45 | 15/10.4 | ℄/14.0 | 22/14.4 | 30-40/15.4 Rock

Turn Top of Stake
8.69 L of ℄ Sta. 178+00

1.47 1137.67

11.95

0.22 1125.94

Rock 1120.4

178+50 | 35/0.5 | 25/0.5 | 13/2.3 | 8/6.2 | 5/5.8 | ℄/5.5 | 16/5.4 | 21/5.9 | 24/4.1 | 25/4.4 | 35/4.4

~~10.78~~

9.27 1116.67 1116.69 ~~1116.69~~

13.08 Turn

References on PC 183+82.34
Iron pipe

85.35

19.50

S+W in S side 30" Maple

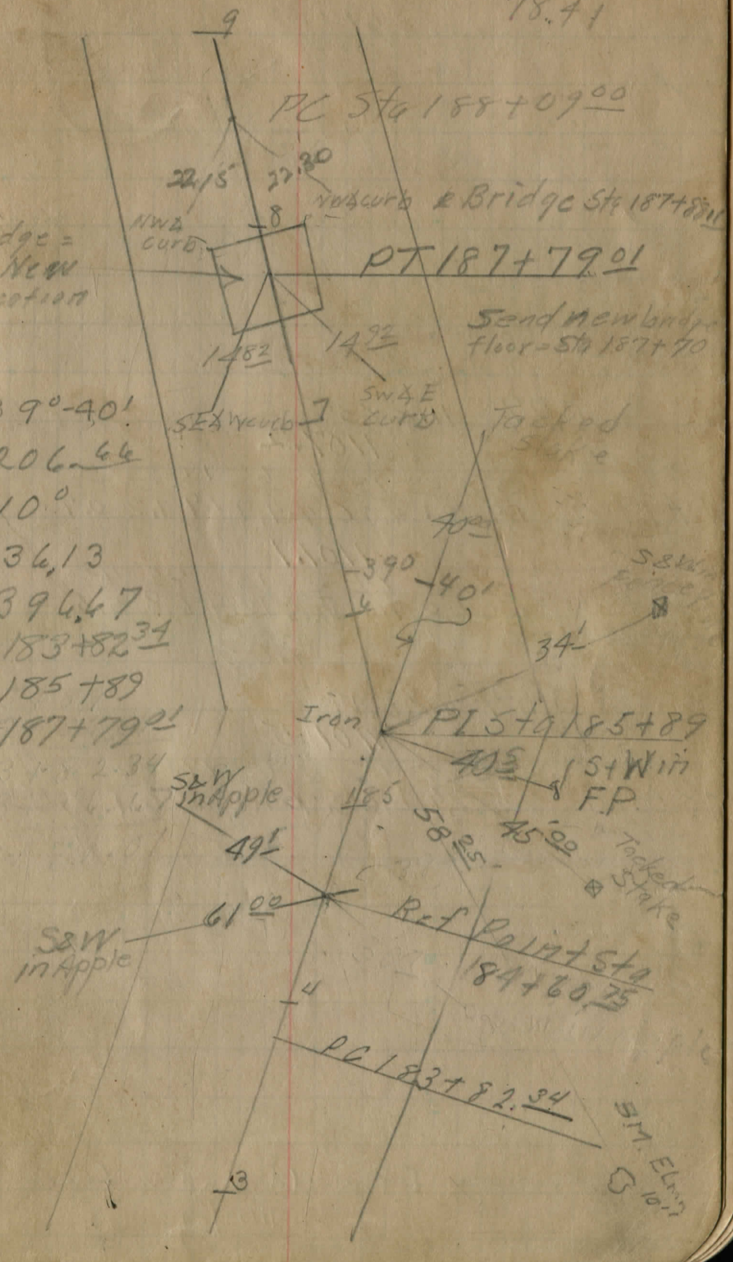
S+W S side Apple

184.99
183.82.34

22.48 22.50

8460.75
8382.34
78.41

Δ = 39°-40'
T = 206.66
D = 10°
E = 36.13
L = 396.67
PC = 183+82.34
PI = 185+89
PT = 187+79.01



8°-30' = 100
4-15' = 50
2° 07' = 25'

2°-07'-L
4-15
6-22 -
4-15
10-37 -
4-15
14-52 -
3-29
17-82
17-21

0.79 1113.65'
1107.2

	25	35	20	13	8	6	19	25	35
179+00	1.9	2.1	4.7	6.4	4.9	1.9	1.2	0.7	

1101.1

	30	25	14	8	15	25	40	
179+50	6.0	6.8	9.0	12.5	12.4	6.8	5.6	

9.03

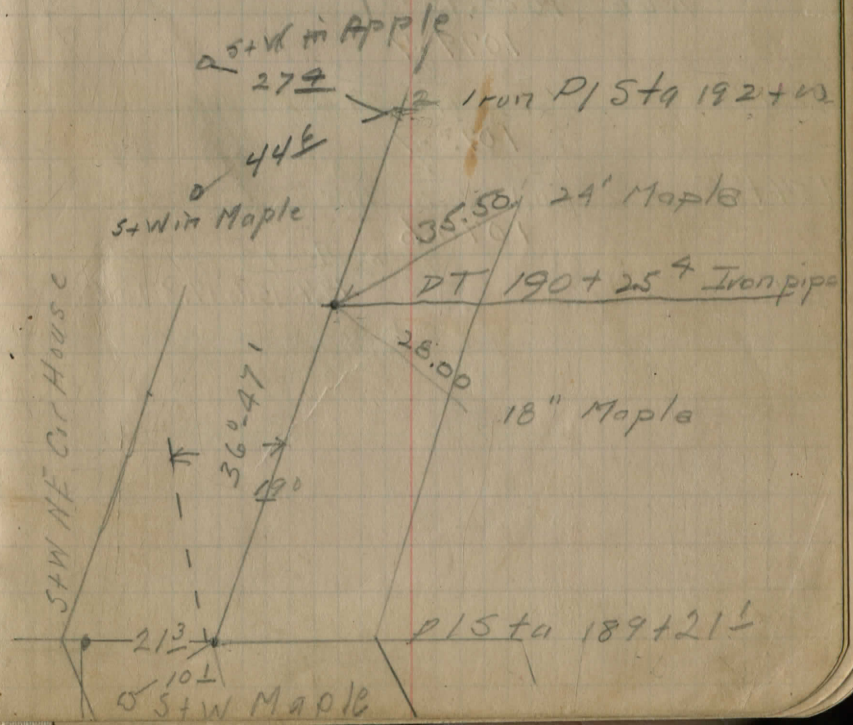
0.57 1105.19
1101.5

	40	25	15	8	15	19	24	35
180+00	3.2	3.9	3.6	3.7	4.0	3.8	6.1	8.5

I.P. in fd. under fence
11/13/69

Δ = 36°-47'
D = 17°
T = 112.1
E = 18.2
L 216.4
PC = 188+09.2
PI = 89+21.1
PT = 190+25.4

1°20' → Sta 192+00 PRC
Bobeau Survey
= Sta 192+20.7
New Relocation



1097.9

181+00 — 25: 7.1; Q: 7.3; 21: 7.2; 33: 8.0; 45: 8.8

1094.2

182+00 — 35: 11.0; 26: 14.5; 14: 14.0; Q: 14.0; Q: 11.0; 25: 16.4

11.85

2.02 1095.36

1088.2

183+00 — 25: 6.7; Q: 7.2; 9: 13.5; 21: 12.2; 32: 13.1; 40-50: 7.5

13.09

1.66 1083.93

1079.7

184+00 — 35: 3.3; Q: 4.2; 25: 5.2

1073.9

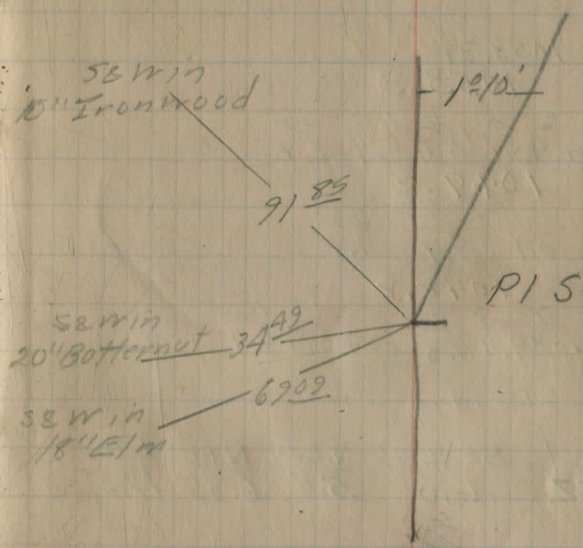
184+75 — 35: 10.1; Q: 10.0; 25: 11.8

1070.6

185+00 — 25: 13.0; Q: 13.3; ~~4: 13.4~~; 13: 15.6; 25: 17.8; 35: 18.9

12.93

Δ = 1°-10' R.



Δ = 1°-20' L

D = 0°-45'

~~T = 83.35~~ T = 88.85

Ext = .51

~~R = 7736.0~~ R = 7633.16

L = 177.72

CORRECTION 11-24-69 CR

Sta 192+00 PI

1.09 1072.29

13.15

3.96 1063.10

8.53 1054.57 ~~1054.56~~ 1054.56

3.78 1058.34

1053.3

185+50 25 4.6 20 4.4 8 5.6 8 5.0 13 5.3 25 6.4

1049.2

186+00 25 10.1 9 9.1 25 7.4

1048.8

187+00 25 11.2 14 10.2 9 10.8 3 9.4 8 9.5 8 8.7 13 8.7 10 9.1 25 10.2

Bridge

SAb 7.52 SE. Bridge 6.0 N.E.B. 5.5 NAb 6.85 FL 17.5

1052.3

187+90 8 6.0 Level

5.20 1053.14 1053.09

9.88 1063.02

1062.9

188+00 10.1 Level

1056.9

189+00 25/3.8 6/5.0 3/6.2 6.1 10/5.9 15/6.8 20/6.5 25/7.0

1059.7

190+00 25/4.2 11/4.0 8/3.4 6/3.3 13/3.8 19/3.3 25/2.9

1059.8

191+00 25/4.0 10/3.3 6/3.2 10/3.4 25/3.7

29	Rt	177+00
~~26~~	~~Rt~~	176+50
12	Rt	176+00
7	Rt	175+50
7	Lt	173+50

all in the stakes ℄ Rd. ℄

Datum ℄ of Old Road.?

Dist	Location	Sta
0		192+00
0		191+00
3'	Rt	190+00
3	Rt	189+50
3	Rt	189+00
0	0	188+50
0	0	188+00
0	0	187+00
15	Rt	186+50
35	Rt	186+00
60	Rt	185+50
85	Rt	185+00
58	Rt	184+00
32	Rt	183+00
12	Lt	182+00
41	Lt	181+00
85	Lt	179+50
73	Lt	179+00
8	Rt	178+50
41	Rt	178+00
40	Rt	177+50

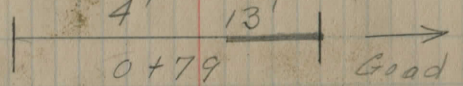
Sta.

0+00
+50
1+00
+50
2+00
+50
3+00
+50
4+00
+50
5+00
+50
6+00
+50
7+00
+50
8+00
+50
9+00
+50
10+06

Culvert Data

Sta 0+00 at cross Road Culvert should be 60' Long or 40' Long set back 40'

12 CSP Sta 0+79



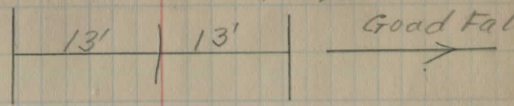
℄ Sta 1+00 = 3.40

Build new 24" YSP.

Fl	℄	Fl
6.4	3.9	6.7

Note at sta 19+00 Give prop Rt 30' tile or 18" Corr drive.

Sta 22+20



Sta 22 = 5.3

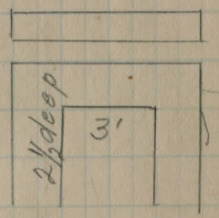
Fl	13	12	℄	12	13	Fl
8.4	3.1	4.9	4.9	5.3	4.0	8.6

· Dirt Floor

Stone Culv.

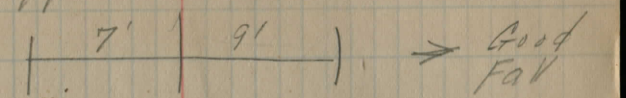
Would advise std.

3' by 3' Hillside Culv.



Sta 47+31

12" CIP



Build new 18" Hillside

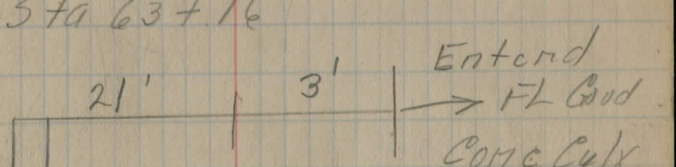
48+00 = 6.8
FL 5.7 — P 4.6 — FL 7.6

Clean Channe both sides

Sta 52+50 Left Pethibone Road.

Either allow 200 Cuyds Exc. to turn water west along road or build 24 Side Road Culv 40' Long.

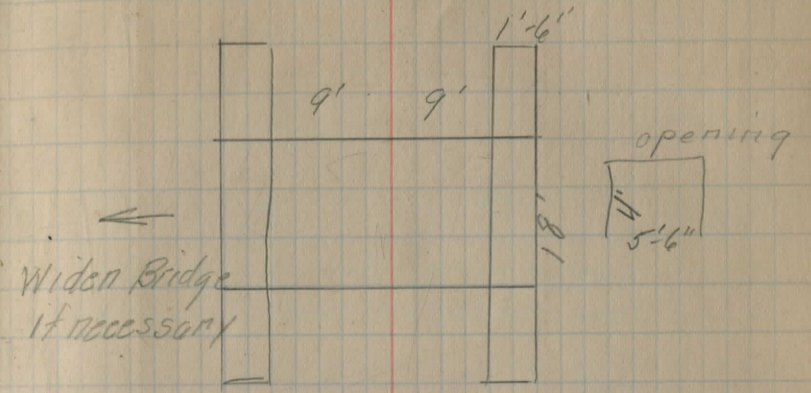
Sta 63+16



63+00 = 5.4
FL 8.4 — 21 4.5 — 20 5.2 — P 5.4 — 3 5.1 — 3 4.5 — FL 7.5

2'-6 by 2' Hillside Culvert
Extend Rt.

Sta 68+58

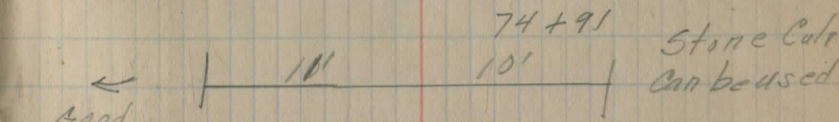


69+00 = 43

FL						
9.2	3.1	4.1	4.0	4.0	3.2	9.1

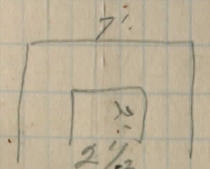
Conc Headwall + Floor stone Abut and Box

74+91



75+00 = 4.4

FL						
8.2	4.5	5.0	4.6	5.5	4.5	7.9



Sta 79+61 Side Road
Culv. Right 40' Long

12" CIP
16' 10' Sta 80+25

80+00 = 57
FL 9.1 4 5.4 FL 4.8

~~Note either Build Side Road~~
~~Culv. or Hillside at Sta 80+25~~
Build side Road Cut out Culv 80+25

Sta 82+43

Good Fall 82+00 = 54 20" CIP
FL 8.1 4 ~~4.6~~ 4.8 FL 7.0

Build new 24" Hillside here.

Sta 94+02
Build new 18" VSP Culv.
Good Fall
10' 12" Drain

94+00 5.6
FL 10.0 4 5.5 FL 9.1

Sta 100+24

deep ravine ← 10" C.I.P.

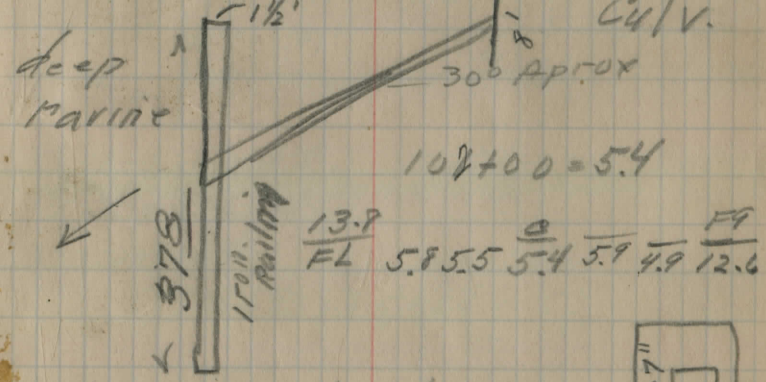
Locate new 18" Culv. Sta 100+40

Sta 100+00 = 5.25

FL. 11.9 | E 5.7 | FL 7.9

Note Keep these Flow Line at Approx. Same Elev.

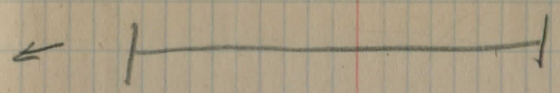
Sta 102+66 Stone Culv.



Keep EL about same

Leave stone Headwalls to hold Fill Extend Culvert. for Fill Sec.

Sta 123+24

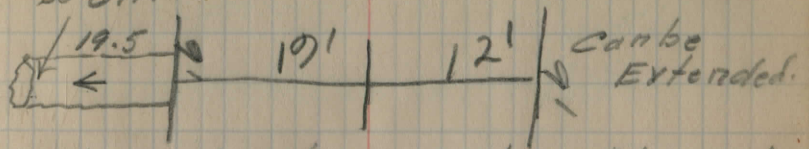


123+40 = 51

100 / 9.5 | FL 6.0 | E 5.3 | FL 7.7

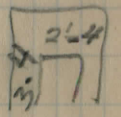
Build new Std 18" R.S.P.

30" C.I.P. Sta 134+84 Stone Culv.



Extend culvert 35' from ℄ to Left. for sidewalk

Clean Channel.

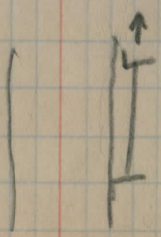


Sta 135+00 = 53

FL 12.1 | 5.4 | 6.0 | E 5.7 | 2.3 | 5.7 | FL 11.2

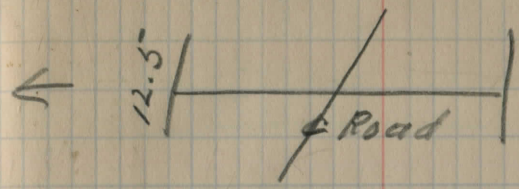
Sta 146+48

Build side Road Culv Rt side



Build new

Sta 147 + 15



Stone Culv can be used.

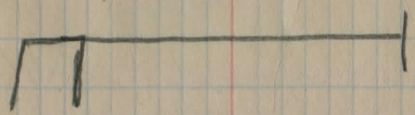
Sta 147 = 54

FL 8.2 — 3.4 — 4.8 — ℄ 4.9 — 4.1 — 3.7 — FL 8.5

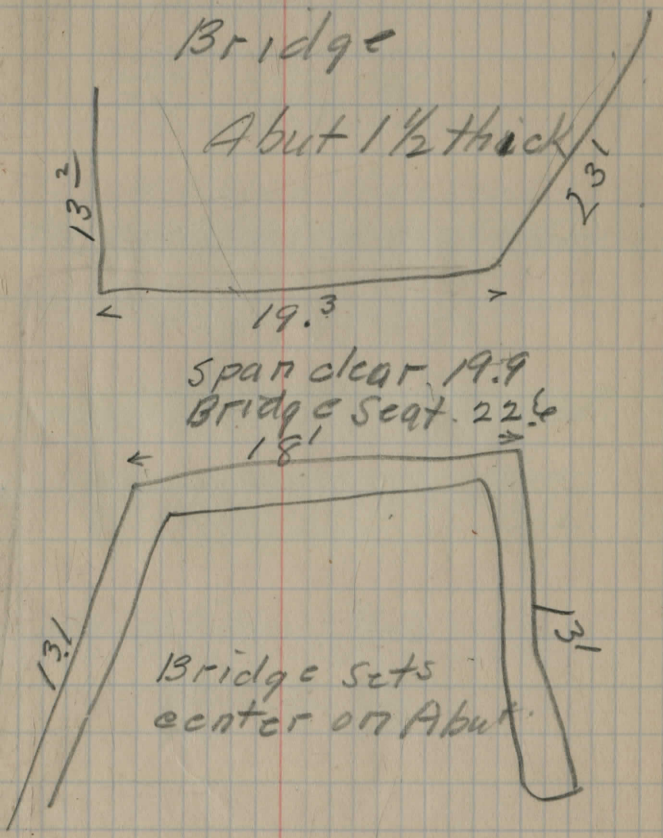
2-5 by 2-5

Sta 179 + 50

Build 3 by 4 Box Hillside.

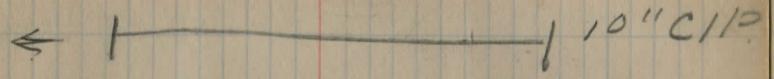


Sta 186+45
check see if 24" Side
Road needed



Cut Out

Sta 191+28

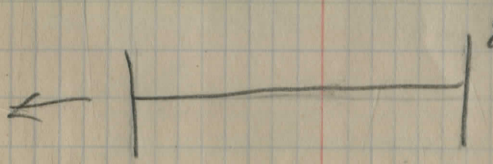


191+00 = 6.3

FL 7.4 | E 5.7 | FL 7.1

Use Hillside if necessary try and eliminate Culv.

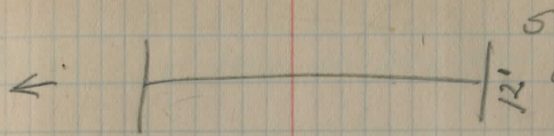
Sta 195+80



Sta 195+00 = 4.0

FL 7.2 | E 5.8 | FL 6.9

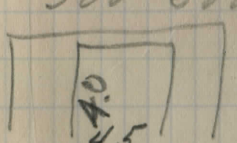
Sta 198+26



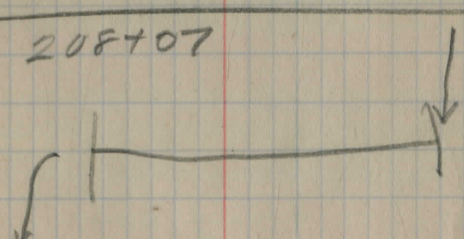
198+00 = 4.9

FL 11.0 — 4.0 — 7.4 — D 4.0 — 7.1 — 3.8 — FL 10.9

Either put this Culv about 300' South or build Culv Sta 195+80 Extend if used



208+07



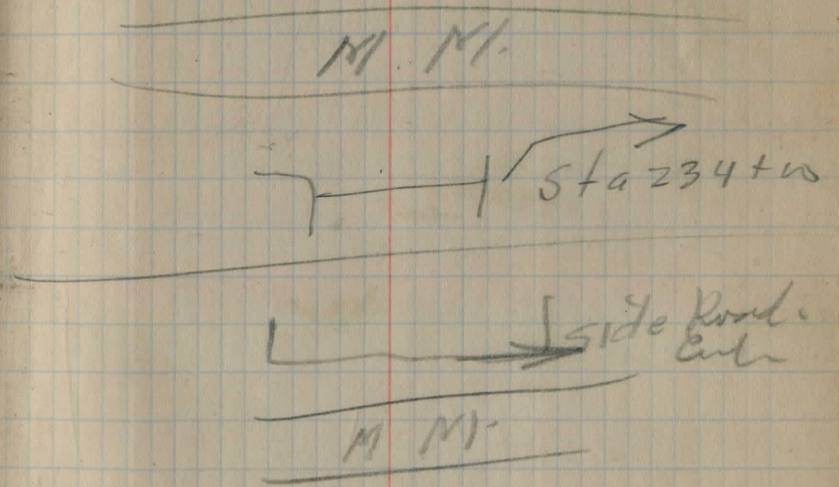
Build new 18" Hillside

208+00 = 8.6

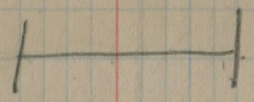
FL 9.0 — D 8.0 — FL 8.6

Sta 234+95

Side Road Culv from Main Market



Sta 245+09

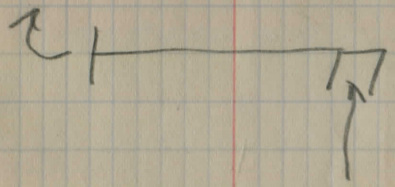


St. 245+00 = 4.8

FH			E			FL
6.9	3.7	5.0	4.6	3.9	3.6	7.0

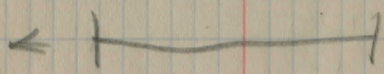
Cut this auto-cut.
Does not work at present.

Sta 248+76
Build new 12" VSP.



Sta 253+59

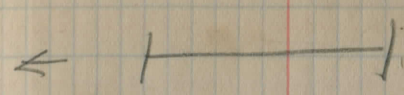
12" CIP



253+00 = 5.5 Cut channel.

100		E	
7.3	FL 6.9	4.8	FL 4.5

256+37

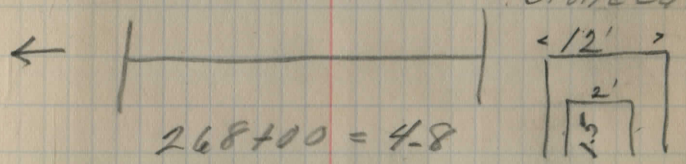


102 / 7.7 — FL / 6.8 — 256 = 49 — 2 / 5.1 — FL / 6.4

Clean Channel

268+04

Stone Culv.



268+00 = 4.8

160 / 7.4 — FL / 7.0 — 3.0 — 4.6 — 4 / 4.6 — 4.7 — 3.4 — FL / 7.1 — 200 / 5.6

Clean Channel

Build new 2' by 2'

	Rod	
194+00	1063.74	
193+00	1063.62	
+50	1063.36	
192+00	1062.71	7.65
+50	1061.66	
191+00	1060.62	4.68
+50	1058.58	
190+00	1056.94	8.36
+50	1055.30	
189+00	1053.66	8.22
+50	1052.41	
188+00	1051.95	

21.1		20.1			26.5	27.5
20.0		19.0			25.7	26.7
F0.6						F0.9
23.8		22.8			21.0	22.0
F1.5						F0.8
20.9		19.9			20.2	21.2
C2.8			14.9			C3.3
15.7		15.7			25.2	26.2
C5.5			15.9			C2.7
20.9		19.9			25.7	26.7
			10.0	11.7		
24.1		23.1			27.5	28.5

	Elev	B.M.	B.S.	H.I.	
		1054.56			
			3.19	1057.75	
+50	1052.26				
					0.09
187	1053.36	2.18	12.94	1070.66	
					0.73
+50	1055.24		11.55	1081.42	
					0.50
186	1057.92	-0.17	12.62	1093.54	
+50	1061.36	-3.61			
185	1065.59	Rt 5.01	Lt 15.83		
+50	1070.21				
184	1074.84	6.58			
+50	1079.46				
183	1084.08	9.46			
+50	1088.70				

		12.9		
F6.3 34.5	33.5	13.6	28.4	F5.0 29.4
		13.0		
F10.0 40.2	39.2	13.0	29.8	F6.8 30.8
F6.7 36.2	35.2	13.0	36.8	F8.9 37.8
C6.0 34.0	33.0	13.0	22.3	C0.8 23.3
		13.0		
		12.2		
C6.1 35.0	34.0		26.0	C4.0 27.0
		9.5		
C3.9 30.3	29.3		20.7	21.7

7' Berm 185+25 to 187+50

1093.54

0.97

		9.07	1101.64	
182	1093.33	LL 0.21 RM 8.31		
+50	1097.95			
181	1102.57	-0.93		
+50	1107.19			
180	1111.82	-6.09		
+50	1116.44	0.35		
179	1121.06	-4.27		
+50	1125.68	2.53		
178	1130.31	7.59		
+50	1134.94	12.31		
177	1139.57	7.68		

F1.2 / 19.5	18.5	L+ 9.1	24.6	C1.6 / 25.6
F4.5 / 27.1	26.1	10.9	25.8	F4.7 / 26.8
		11		
F10.2 / 37.5	36.5	11	44.9	F12.2 / 45.9
F11.2 / 34.8	33.8	11	33.3	F9.5 / 34.3
F6.5 / 36.2	35.2	11	31.5	F5.7 / 32.5
F1.3 / 26.0	25.0	11.	24.8	F1.5 / 25.8
C5.5 / 30.8	29.8	11.0	21.6	F0.7 / 22.6
C6.7 / 25.3	24.3	11.0	24.8	F0.1 / 25.8
C7.9 / 26.0	25.0	11.0	22.0	C2.2 / 23.0

7 1/3 Berms 178 to 181 +50

special Slope 173+50 to 178

5 1/3 Berms Sta 170 to 195

+50	1144.19	13.94
176	1148.82	9.11
+50	1153.45	13.70
175	1158.08	9.12
+50	1162.70	13.04
174	1167.33	8.41
+50	1171.95	11.78
173	1176.58	7.15
+50	1180.75	2.98
172	1184.00	6.18
171+00	1187.70	2.48

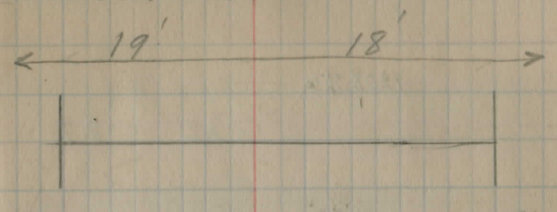
C 5.8						C 3.3
26.0	25.0	11.0		22.0		23.0
C 6.2						C 2.6
24.5	23.5	11.0		23.0		24.0
C 7.3						C 7.2
26.0	25.0	11.0		26.3		27.3
C 7.2						C 7.2
24.5	23.5	10.1	9.3	23.0		24.0
C 5.8						C 6.1
22.0	21.0		11	28.2		29.2
C 3.2						C 6.0
21.2	20.2		13	30.3		31.3
E 1.5						C 4.7
20.2	19.2		13	29.9		30.9
C 0.0		tost q 178				C 4.6
20.4	19.4	½ to1 Lt 1 to1 Rt	13	29.2		30.2
C 2.6						C 1.6
20.7	19.7	½ to1 Lt 1 to1 Rt	Rt 13.0	26.7		27.7
C 0.7						C 0.8
21.5	20.5		Rt 10.2	23.4		24.4
E 1.6						E 1.7
20.7	19.7			20.4		21.4

	H.I	L Side	R Side
	1194.20	C-2.5	C-2.2

Sta	+S	H.I	L.S	R.S	
	0.55	1203.73			BM #30 1203.18
			5.33	4.53	
			C-1.4	C-1.7	

	H.I	L.S	R.S.
	1203.37		
		C-2.0	C-2.3

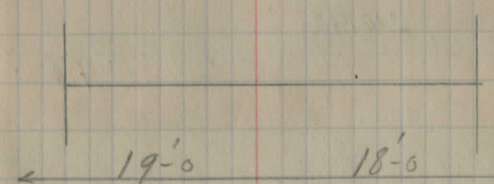
Sta. 268+04



FL = 1187.5
FL
C-2.5

FL Elev. 1188.0
FL
C-2.2

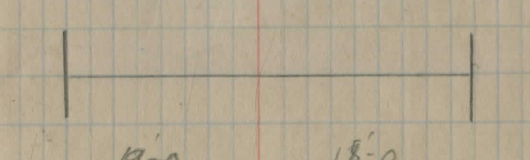
Sta 257+50



FL - 1197.0
FL
C-1.4

FL Elev 1197.50
FL.
C-1.7

Sta. 253+59



FL. 1196.0
FL
C-2.0

FL
C-2.3

FL. 1196.5

Sta.		H.I	L.S.	R.S.	
248+76					
		1208.16			
			C-3.2	C-3.7	

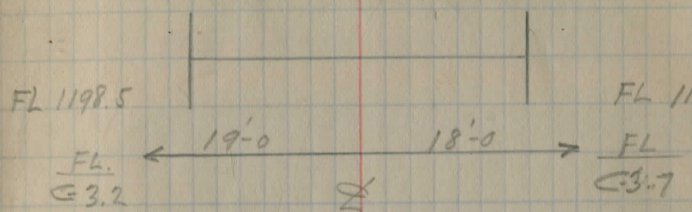
Sta.	+S	H.I	L.S	R.S	BM. 28 1207.59
235+25	3.33				
		1210.92			
			C-2.6	C-4.1	

	+S	H.I	L.S	R.S.	BM #28 1207.59
	4.22				
		1211.81	C-4.4	C-5.0	

3.2 / 4.8 / 8.0

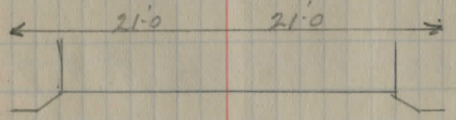
3.7 / 3.8 / 7.5

Sta. 248+76



Culvert Nth. Main Market

Sta. 235+25



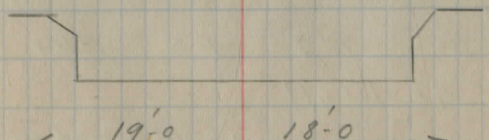
FL Elev 1203.00

FL
C-2.6

FL Elev 1202.50

FL
C-4.1

Sta 234+00



FL 1203.00

C-4.4

FL 1202.50

C-5.0

New Bench

Sta 197+80

Spike in Root Maple 35' Lt

℄ Elev 1063.32

~~1066.~~

1063.32
2-66
1065.97

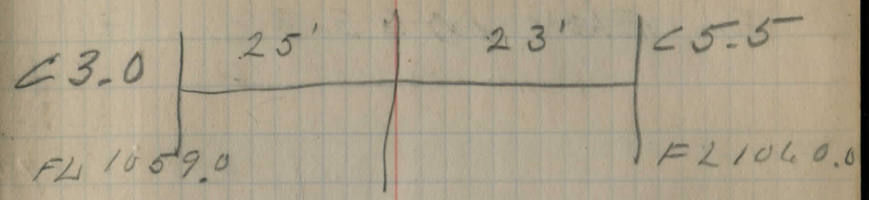
1065.97
9-20
1056.70

1065.97
1060.50
5.47
4.77
.70

1065.97
1060
5.97
5.47

BS	HI	FS	Elev	BM #20
0.42	1117.11			1116.69
		12.75	1104.36	
3.99	1108.35			
Rod R		8.85	C3.0	Fl. 1096.5
Rod L		10.85	C5.5	Fl. 1097.5

Sta 198+10



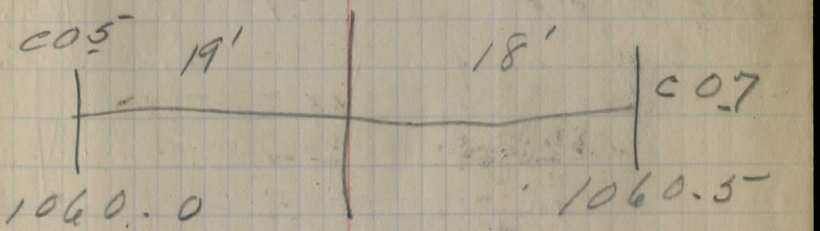
1066.87
2.47
1069.34

1069.34
1059
10.34
7.34

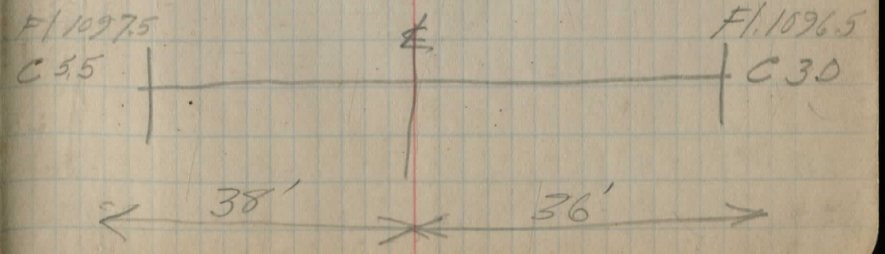
1069.34
1060
9.34
3.84
5.50

1069.34
6.02
1063.32

Sta 195+80



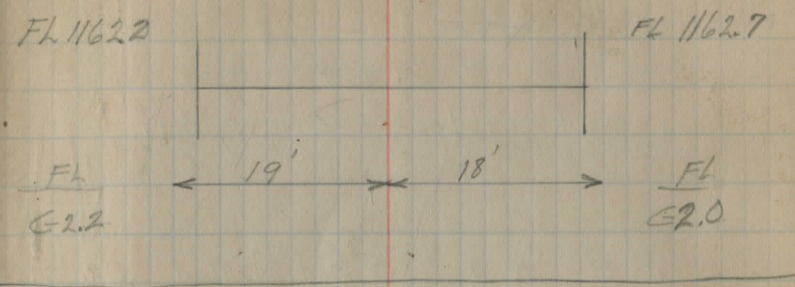
Sta 180+00



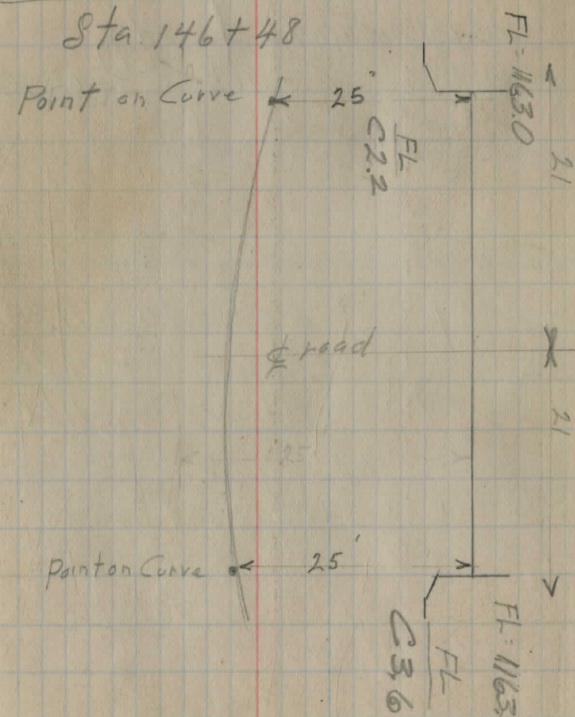
USGS BM on Stone Col

Sta.	B.S.	H.I.	Grade Rod	F.S.	Elev 1166.18
	5.20	1171.38			
Rod R			8.68	6.68	1162.70
Rod L			9.18	6.98	1162.20
				Elev	1166.18
	B.S	H.I	Grade Rod	F.S.	
	5.42	1171.60			
			18.60		1163.0
Rod N				6.40	C2.2
			8.10		1163.5
Rod S				4.50	C3.6

Sta 147+15



Sta 146+48



B.M #15
N.W. Cor. Hdwl
Elev
1154.01

B.S.	H I	Rod L	Rod R.
5.08	1159.09		
		9.59	8.39

Look back of book For New B.M.

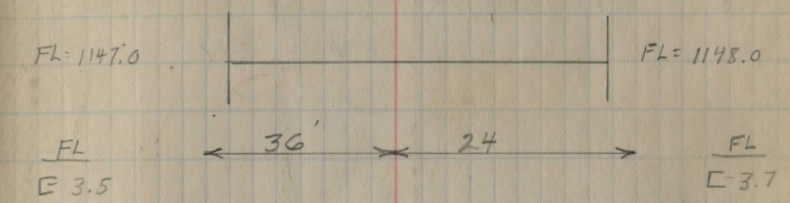
B.S.	H I	G Rod	G Rod	BM #24
				1164.06
		10.5	10.6	

Changed to Sta 205+75

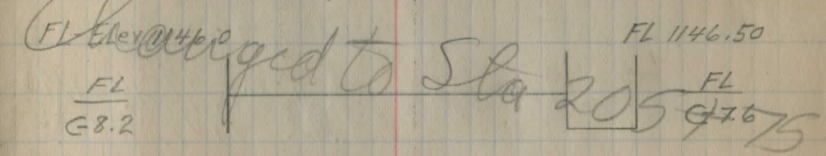
Sta 205+75 ℄ Grade - 1129.47
Flow R - 1126.7
Flow L - 1126.2

	BS	HI	FS	Flow	Stake Rod
		1133.08			
R			6.38	1126.7	1.98
L			6.88	1126.2	0.38

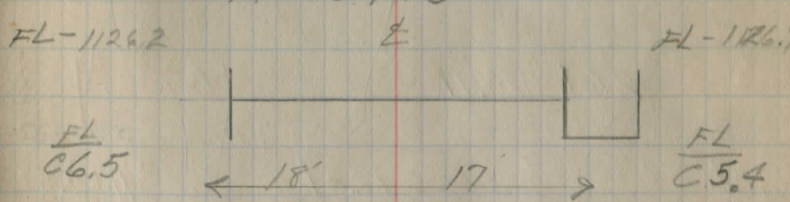
Sta 134+80



Sta 208+07



Sta 205+75



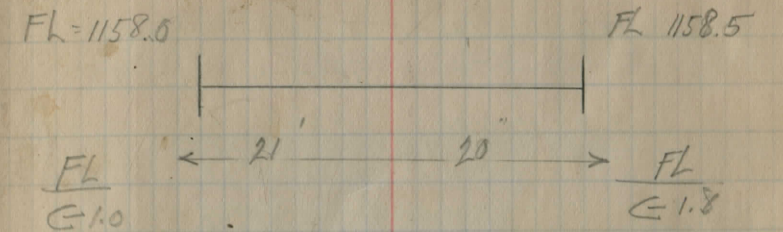
B.M. 13

	B.S.	H.I	G Rod	Rod	
					1163.86
	2.12	1165.98			
R			7.48	5.68	C 1.8
L			7.98	6.98	C 1.0

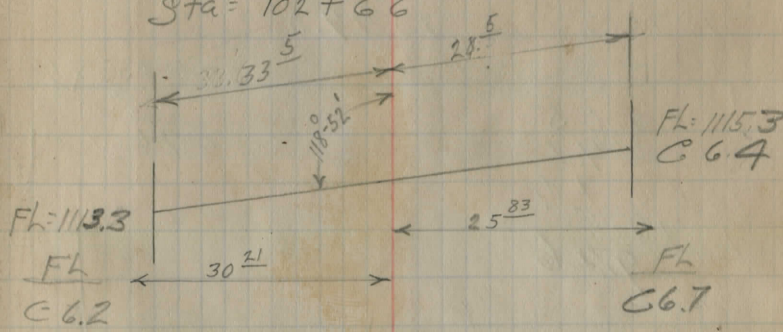
	B.S.	H.I	G Rod	Rod	
					New B.M. #11 1126.00
	0.72	1126.72			
R. Side			11.42		1115.30
				5.02	C 6.4
L Side			13.42		1113.30
				7.22	C 6.2

	B.S.	H.I	G. Rod	Rod	
					B.M. #11 Elev 1122.10
	2.61	1124.71			
Right			7.91		1116.80
				5.21	C 2.7
			11.59	1113.12	
	3.15	1116.27			
			10.27		1106.00
Left				8.77	C 1.5

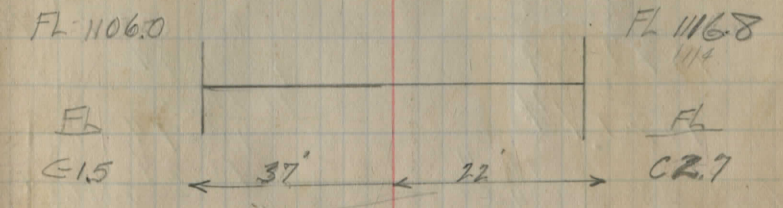
Sta. 123+26



Sta = 102+66



Sta. 100+40



B.M. # 10

Elev. Stone.

	B.S.	H.I	G.Rod	Rod	1110.27
	3.51	1113.78			
			12.87	1100.91	T.P
	5.39	1106.30			
Rod R			9.80	5.20	E 4.6
L Side			10.3	8.10	C 2.2

Sta 94+02

Fl: 1096.0 Fl: 1096.5

Fl E 2.2 Fl C 4.6

31' 30'

Sta 82+43 Hillside

18' x 17' C 3.0

1076.5 1077.0

1085.05 4.1 1065.74 1070.50 9.26

1085.76 9.00 1076.76

1085.76 6.53 1079.23 2.51 1081.74

1081.74 1071.00 10.74

1081.74 4.5 4.2 9.3 10.24

1081.74 4.5 87.24

1076.20 2.75 1073.45

10.24 4.82 5.42

1075.20 2.75 1072.45

1081.74 9.3 1072.44

Road

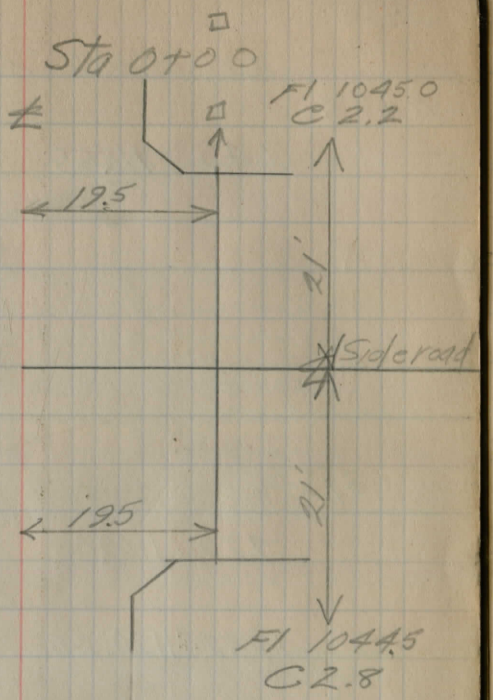
22'

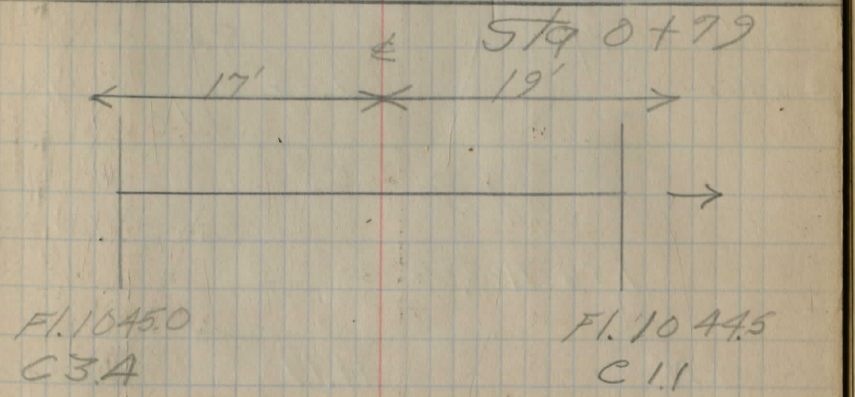
C 2.0 21' 21' C 4.5

6/13/28. Richey Whistin Parks Spohn

	BS	HI	Grade Rod	FS	
BM #1					1045.55
	6.85	1052.40			
Grade S			7.40		1045.0
				5.20	C2.2
Grade N			7.90		1044.5
				5.1	C2.8

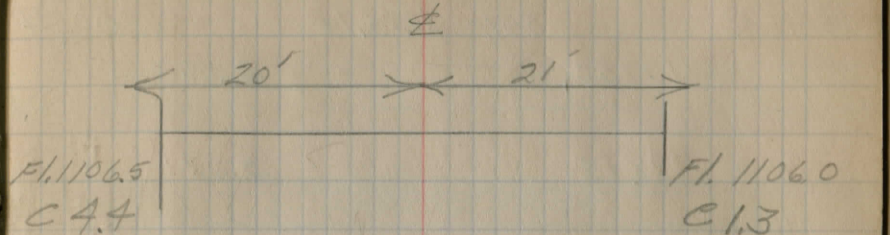
	BS	HI	Grade Rod	FS	
BM #1					1045.55
	6.66	1052.21			
Grade E			7.71		1044.50
				6.61	C1.1
Grade W			7.21		1045.00
				3.81	C3.4





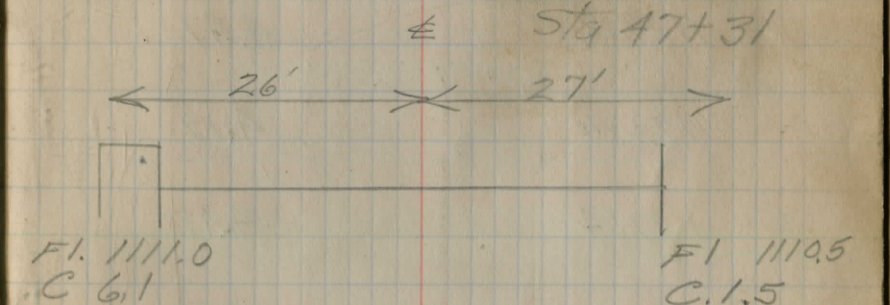
	BS	HI	Grade Rod	FS	
BM #3					1112.20
	3.45	1115.65			
Grade R			9.65		1106.00
				8.35	C 1.3
Grade L			9.15		1106.50
				4.75	C 4.4

Sta 22+20



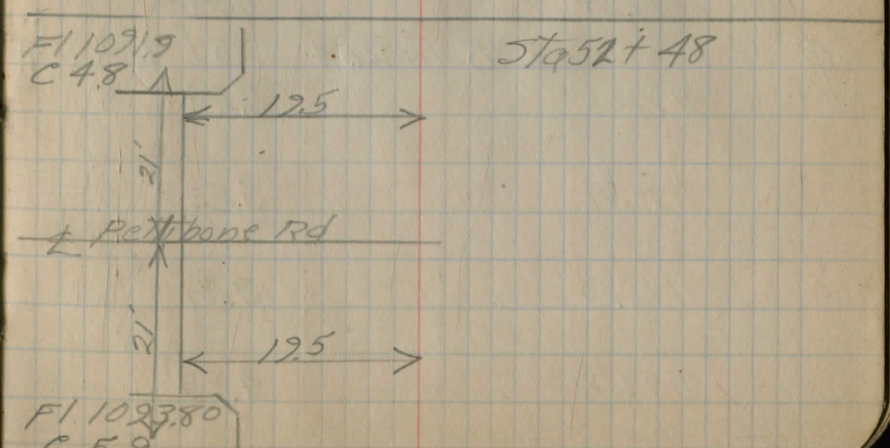
	BS	HI	Grade Rod	FS	
BM #6					1101.83
	7.20	1109.03			
			0.10	1108.93	
	11.32	1120.25			
Grade R			9.75		1110.50
				8.25	C 1.5
Grade L			9.25		1111.00
				3.15	C 6.1

Sta 47+31



	BS	HI	Grade Rod	FS	
BM #6					1101.83
	1.86	1103.69			
Grade N			11.79		1091.90
				6.99	C 4.8
Grade S			9.89		1093.80
				3.99	C 5.9

Sta 52+48



7/9/28

Richey Parks
Whiskin Spohn

Fine Grade

Sta	Grade	BS	HI	FS	
BM #32		3.51	1203.75		1200.24
282	1197.50			6.25 ✓	
+50	1198.13			5.62 ✓	
281	1198.75			5.00 ✓	
+50	1199.28			4.47 ✓	
280	1199.56			4.19 ✓	
+50	1199.64			4.11 ✓	
279	1199.50			4.25 ✓	
+50	1199.25			4.50 ✓	
BM #32		1.78	1202.02	3.51	1200.24
278	1199.00			3.02 ✓	
+50	1198.71			3.31 ✓	
277	1198.33			3.69 ✓	
+50	1197.77			4.25 ✓	

Sta	Grade	BS	HI	FS	
			1202.02		
276	1197.32			4.70 ✓	
150	1196.75			5.29 ✓	
275	1196.15			5.87 ✓	
+50	1195.57			6.45 ✓	1195.57 ✓
		2.07	1197.64		
274	1194.98			2.66 ✓	
150	1194.40			3.24 ✓	
273	1193.82			3.82 ✓	
+50	1193.24			4.40 ✓	
272	1192.66			4.98 ✓	
+50	1192.14			5.50 ✓	
271	1191.73			5.91 ✓	
+50	1191.42			6.22	
		3.74	1195.14	6.24	1191.40

6/12/28

Sta	Grade	BS	HI	FS		
			1195.14			
270	1191.25			3.89 ✓		
+50	1191.12			4.02 ✓		
269	1191.00			4.14 ✓		
+50	1190.87			4.27 ✓		
BM #31				4.07	1191.07	1191.05
268	1190.75			4.39 ✓		
+50	1190.63			4.51 ✓		
267	1190.50			4.64 ✓		
		5.55	1196.03	4.66	1190.48	
+50	1190.46			5.57 ✓		
266	1190.63			5.40 ✓		
+50	1190.96			5.07 ✓		
265	1191.50			4.53 ✓		
+50	1192.21			3.82 ✓		

Sta	Grade	BS	HI	FS		
			1196.03			
264	1193.13			2.90 ✓		
+50	1194.21			1.82 ✓		
263	1195.50			0.53 ✓	1195.50	
		9.31	1204.81			
+50	1196.87			7.94 ✓		
262	1198.12			6.69 ✓		
+50	1199.11			5.70 ✓		
261	1199.85			4.96 ✓		
BM #30		1.59	1204.77	1.59	1203.22	1203.18
+50	1200.33			4.44 ✓		
260	1200.55			4.22 ✓		
+50	1200.51			4.26 ✓	1200.51	T.P.
259	1200.44					
+50	1200.27					

6/15/28 Richey Whitsitt Parks Spohn

Rock Sections

	BS	HI	FS	
BM	6.34	1164.40		1164.06
	0.51	1152.75	12.16	1152.24
	0.80	1141.37	12.18	1140.57

206

1133.4

206+25 — 15/8.2 12/8.6 E/5.0 7/8.3 16/8.0

1136.1

206+50 — 16/5.1 13/5.7 11/6.2 E/5.3 13/5.3 19/5.2

1138.1

206+75 — 15/4.0 12/3.9 E/3.3 13/3.3

1141.1

207+00 — 16/2.3 10/0.5 E/0.3 9/1.4 13/0.9 16/0.7

11.63 1152.20 0.80 1140.57

1142.6

207+25 — 17/10.0 12/9.5 E/9.6 5/8.9 11/8.9

1144.2

207+50 — 16/8.1 E/8.0 Level

1146.2

207+75 — Level E/6.0 — level

1148.8

208+00 — Level 8/4.0 4/3.7 E/3.4 6/3.5 12/3.0

1150.7

208+25 — 8/1.3 E/1.5 13/1.3

0.57 1151.63

11.62 116325

Rock only in ditches X Sect shows same

116325

1153.0

208+50 $\frac{8}{10.1}$ $\frac{\text{℄}}{10.3}$ $\frac{8}{10.4}$ $\frac{14}{10.6}$

1155.8

208+75 $\frac{20}{5.6}$ $\frac{15}{7.6}$ $\frac{8}{7.6}$ $\frac{\text{℄}}{7.5}$ $\frac{7}{7.8}$ $\frac{12}{8.8}$

1.99 1161.26

5.45 1166.71

BM#24 2.62 1164.09 1164.06

6/19/28 Richey Parks
Whiskin Spohn

Fine Grade

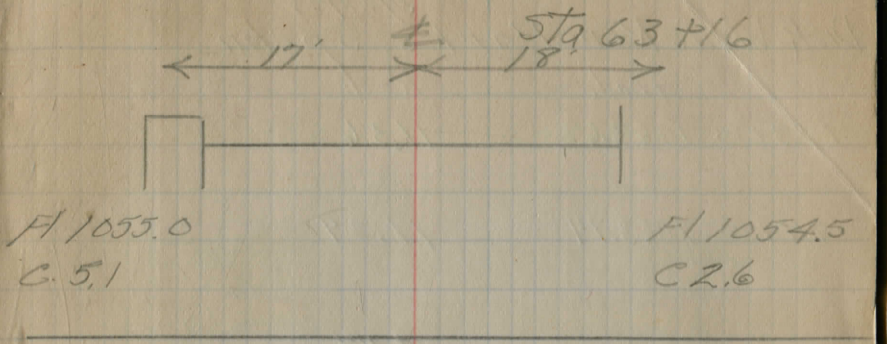
Sta		BS	HI	FS	
BM #31		3.52	1194.51		1190.99
+50	1190.46			4.05	
267	1190.50			4.01	
+50	1190.63			3.88	
268	1190.75			3.76	
+50	1190.87			3.64	
269	1191.00			3.51	
+50	1191.12			3.39	
270	1191.25			3.26	
+50	1191.42			3.09	
		6.15	1197.56	3.10	1191.41
271	1191.73			5.83	
+50	1192.14			5.42	
272	1192.66			4.90	
+50	1193.24			4.32	
273	1193.82			3.74	
+50	1194.40			3.16	

Sta		BS	HI	FS	
			1197.56		
274	1194.98			2.58 ✓	
+50	1195.57			1.99 ✓	1195.57
		6.31	1201.88		
275	1196.15			5.73 ✓	
+50	1196.73			5.15 ✓	
276	1197.32			4.56 ✓	
+50	1197.77			4.11 ✓	
277	1198.33			3.55 ✓	
+50	1198.71			3.17 ✓	
278	1199.00	5.00	1204.00	2.88 ✓	1199.00
BM #32				3.77	1200.23 1200.24
+50	1199.25			4.75 ✓	
279	1199.50			4.50 ✓	
+50	1199.64			4.36 ✓	

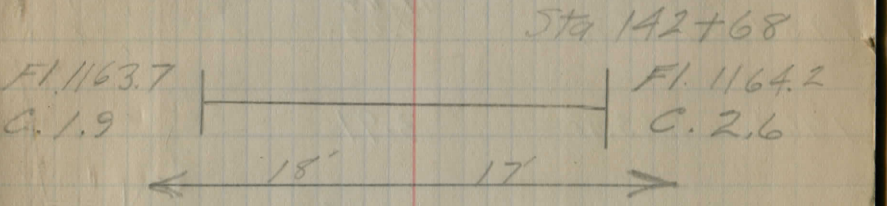
Sta		BS	HI	FS	
			120400		
280	119956			4.44	✓
+50	119928			4.72	✓
281	119875			5.25	✓
+50	119813			5.87	✓
282	119750			6.50	✓

6/19/28

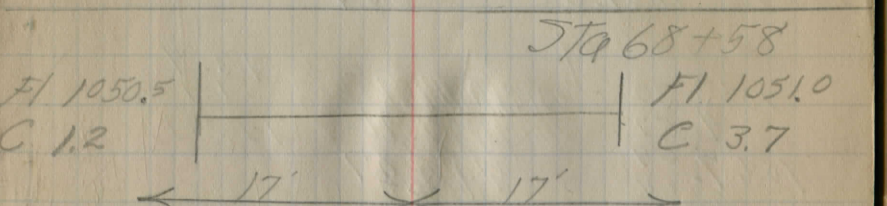
BM #7	3.47	1060.28			1056.81
"	6.16	1062.28	4.16	1056.12	
	1.16				
Right			7.78		1054.50
				5.18	C 2.6
Left			7.28		1055.00
				2.18	C 5.1



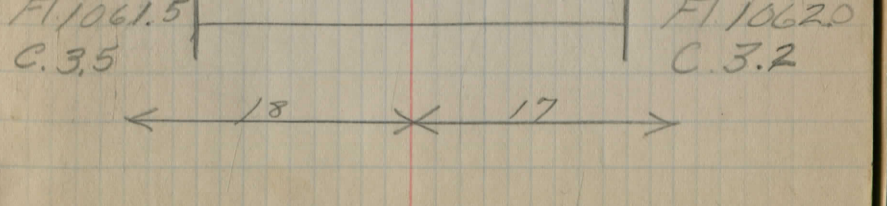
BM #45+00	1.73	1171.04			1169.31
Flow R			6.84		1164.20
Stake R				4.24	C 2.6
Flow L			7.34		1163.70
Stake L				5.44	C 1.9



BM #7	4.03	1060.84			1056.81
Flow R			9.84		1051.00
Stake R				6.14	C 3.7
Flow L			10.34		1050.50
Stake L				9.14	C 1.2



BM #	5.00	1071.31			1066.31
Flow R			9.31		1062.00
Stake R				6.11	C 3.2
Flow L			9.81		1061.50
Stake L				6.31	C 3.5



Slope Stakes
5/22/25

Dick Whisker Parks Spohn

	Grade	Rod
193+00	1063.62	11.36
194+00	1063.74	11.24
195+00	1063.84	11.13 / 4.03
196+00	1063.98	3.91
197+00	1064.44	3.45
198+00	1067.32	0.57

1063.32
4.57
1067.89
2.64
1065.25
9.73
1074.98

1074.98
1062.71
12.27

13.4
1.1
12.3

Spike E Road Mark 197+80 35'Lt
1063.32
10' berm 19.3 ditch 23.3 back slope

19.0

C2.2	C2.6		
26.6	27.6		
F1.1	F1.4	C2.6	C2.8
22.2	21.2	27.2	28.2
F5.3	F5.3	C5.5	C4.F
25.7	24.7	32.0	33.0
F3.7	F3.7	F2.7	F2.6
22.5	21.5	19.5	20.5
F2.7	F2.9	F2.4	F2.3
21.3	20.3	19.7	20.7
F3.4	F3.4	F3.2	F3.0
21.9	20.9	20.6	21.6

6/27/28

Richey Whiskin — Parks Spohn

Set by Formula

Sta		BS	HI	FS		
BM #1		8.60	1054.15		1045.55	
0+00	1047.50			6.65		
1+00	1048.72			5.43		
2+00	1049.99			4.16		
3+00	1051.58			2.57		
		7.15	1059.74	1.56	1052.59	
4+00	1053.50			6.24		
5+00	1055.82			3.92		
6+00	1058.55			1.19		
		12.65	1070.93	1.46	1058.28	
7+00	1061.60			9.33		
8+00	1064.97			5.96		
9+00	1068.39			2.54		
		12.76	1081.75	1.94	1068.99	
10+00	1071.81			9.94		
BM #2				6.26	1075.49	1075.48
11+00	1075.23			6.52		

C1.0 / 25.5	C0.8 / 24.5	F0.7 / 22.3	F0.6 / 23.3
F1.3 / 22.2	F1.4 / 21.2	F1.6 / 20.9	F1.4 / 21.9
C0.2 / 24.6	C0.2 / 23.6	F1.5 / 21.1	F1.2 / 22.1
C1.0 / 25.3	C0.7 / 24.3	F0.7 / 22.3	F0.4 / 23.3
F0.7 / 23.0	F0.9 / 22.0	F1.3 / 21.4	F1.3 / 22.4
F1.1 / 22.5	F1.2 / 21.5	F0.9 / 22.0	F0.7 / 23.0
F0.6 / 23.4	F0.8 / 22.4	F1.2 / 21.5	F1.0 / 22.5
C1.5 / 25.9	C1.1 / 24.9	C0.1 / 23.4	C0.2 / 24.4
C2.0 / 27.3	C2.0 / 26.3	C1.8 / 26.0	C2.1 / 27.0
C0.6 / 25.0	C0.5 / 24.0	C0.9 / 24.6	C0.9 / 25.6
C1.6 / 26.4	C1.4 / 25.4	C1.5 / 25.5	C1.8 / 26.5
C2.1 / 27.4	C2.1 / 26.4	C1.7 / 25.0	C2.0 / 26.8

Sta		BS	HI	FS	
			1081.75		
12+00	1078.65			3.10	
		11.23	1089.88	3.10	1078.65
13+00	1082.07			7.81	
14+00	1085.49			4.39	
		8.88	1093.55	0.21	1089.67
15+00	1088.92			9.63	
16+00	1092.34			6.21	
17+00	1095.76			2.79	
		13.10	1110.87	0.78	1097.77
18+00	1099.18			11.69	
19+00	1102.60			8.27	
20+00	1105.92			4.95	
		7.21	1116.06	2.02	1108.85
21+00	1109.08			6.96	
BM #3				6.77	1109.29
22+00	1112.16			3.90	
23+00	1115.24			0.82	
		10.32	1124.39	1.99	1114.07

C0.0 / 24.0	F0.2 / 23.0			C0.7 / 24.3	C0.9 / 25.3
F1.1 / 22.5	F1.2 / 21.5			F1.2 / 21.5	F1.0 / 22.5
F1.5 / 21.8	F1.7 / 20.8			F2.0 / 20.3	F1.8 / 21.3
C2.5 / 27.1	C1.9 / 26.1			C0.0 / 23.3	C0.1 / 24.3
F2.0 / 21.0	F2.2 / 20.0			F3.0 / 19.9	F3.0 / 20.9
F2.1 / 20.7	F2.4 / 19.7			F3.4 / 20.1	F3.5 / 21.1
C2.1 / 27.6	C2.2 / 26.6			F0.3 / 22.9	C0.1 / 23.9
C3.8 / 22.1	21.1	Special L.		C2.7 / 27.3	C2.7 / 28.3
C3.1 / 29.8	C3.7 / 28.8			C3.2 / 28.1	C3.1 / 29.1
C0.3 / 23.9	F0.3 / 22.9			F0.7 / 22.3	F0.7 / 23.3
1109.76					
F2.4 / 20.6	F2.5 / 19.6			F4.1 / 22.1	F4.0 / 23.1
F1.5 / 21.2	F2.1 / 20.2	7' Berm R		F5.8 / 26.5	F5.7 / 27.5

Sta	BS	HI	FS	
		1124.39		
24+00	1118.32		6.07	
25+00	1121.40		2.99	
Sta R			6.59	1117.80
R				

F0.5 / 21.8	F1.7 / 20.7	7' Berm R	F7.5 / 29.9	F7.2 / 30.9
F2.1 / 20.6	F2.5 / 19.6		F3.8 / 21.5	F3.6 / 22.5

6/30/28 — Richey Whitkin — Parks Spohn

Sta		BS	HI	FS	
		12.23	1130.83		1117.80
26+00	1124.52			5.51	
27+00	1127.60			2.43	
		9.73	1139.54	0.22	1129.81
28+00	1130.64			8.90	
29+00	1133.72			5.82	
30+00	1136.80			2.74	
		8.67	1146.56	1.65	1137.89
31+00	1139.85			6.71	
32+00	1142.59			3.97	
		5.13	1148.62	3.07	1143.49
33+00	1144.95			3.67	
BM#4		8.85	1152.90	4.53	1144.09
34+00	1146.91			5.99	
35+00	1148.18			4.72	
36+00	1148.73			4.17	

C2.2 / 27.0 — C1.8 / 26.0 — F1.1 / 21.7 — F0.9 / 22.7

C1.7 / 26.9 — C1.7 / 23.8 — C0.0 / 23.3 — C0.3 / 24.3

C2.0 / 26.8 — C1.7 / 25.8 — F1.2 / 21.5 — F1.3 / 22.5

F0.4 / 23.4 — F0.6 / 22.4 — F0.2 / 23.0 — F0.1 / 24.0

C0.6 / 24.7 — C0.3 / 23.7 — C1.0 / 24.8 — C1.1 / 25.8

C2.6 / 27.4 — C2.1 / 26.4 — C1.4 / 25.4 — C1.7 / 26.4

C2.9 / 28.3 — C2.7 / 27.3 — C1.0 / 24.8 — C1.3 / 25.0 — start of return traverse

F0.1 / 23.7 — F0.4 / 22.7 — F1.9 / 20.5 — F1.7 / 21.5

114.05

F1.0 / 22.2 — F1.4 / 21.2 — F2.6 / 19.4 — F2.4 / 20.4

C0.9 / 24.9 — C0.4 / 23.9 — F1.0 / 21.8 — F0.7 / 22.8

C0.6 / 24.6 — C0.2 / 23.6 — F1.3 / 21.5 — F1.2 / 22.5

Sta		BS	HI	FS	
			1152.90		
37+00	1148.55			4.35	
38+00	1147.73			5.17	
		3.81	1149.24	7.47	1145.43
39+00	1146.54			2.70	
40+00	1144.81			4.43	
41+00	1142.50			6.74	
BM #5				6.48	1142.76
42+00	1139.65				
43+00	1136.22				
44+00	1132.25				
45+00					
46+00					
47+00					
48+00					

F0.2 / 23.3	F0.7 / 22.3		F2.6 / 19.4	F2.5 / 20.4
E1.4 / 21.6	E1.8 / 20.6		F2.5 / 19.6	F2.3 / 20.6
E1.7 / 21.3	F2.0 / 20.3		F2.4 / 19.7	F2.3 / 20.7
F1.0 / 22.4	E1.3 / 21.4		E1.2 / 21.5	E1.1 / 22.5
C1.6 / 26.2	C1.3 / 25.2	1142.76	C0.8 / 24.5	C0.9 / 25.5
—	26.0		25.0	—
—	25.0		25.0	—
—	27.0		25.5	—
—	—		—	—
—	—		—	—
—	—		—	—
—	—		—	—

B.M. X on E. end of gas pump foundation	Elev. 1207.59	
235	1206.00	Rod 3.84
236	1206.00	7.64
237	1206.10	4.54
238	1206.37	4.27
239	1206.74	3.98
240	1207.11	3.75
241	1207.22	3.64
242	1206.75	4.11
243	1206.00	4.86
244	1205.25	5.61
245	1204.50	6.36
B.M. #29 X on S.E. cor of W. headwall culv. Elev. 1204.95		

I.O.F 23.5	22.5	22.1	23.1
F0.3 22.7	21.7	21.8	F0.4 22.8
F0.2 23.3	22.3	22.6	F0.1 23.6
C1.0 23.5	22.5	23.8	C0.3 24.8
F0.4 22.8	21.8	22.2	F0.1 23.2
F0.8 22.7	21.7	22.2	F0.5 23.2
F0.2 23.5	22.5	22.4	F0.2 23.4
C0.5 24.4	23.4	23.5	C0.5 24.5
F0.2 23.3	22.3	24.0	C0.5 25.0
F1.9 20.5	19.5	20.4	F1.6 21.4
F1.8 21.0	20.0	21.3	F1.0 22.3

	Rod	
246	1203.75	3.90
247	1203.00	4.65
248	1202.25	5.40
249	1201.50	6.15
250	1200.75	6.90
251	1200.00	7.65
252	1199.39	2.92
253	1199.04	3.27
254	1198.96	3.35
255	1199.14	3.17
256	1199.46	2.85

F0.1 23.0	22.0		24.2	C1.5 25.2
C1.2 25.2	24.2		26.3	C2.2 27.3
C0.2 23.5	22.5		23.7	C0.7 24.7
F0.4 23.0	22.0		23.6	C1.0 24.6
F1.4 21.2	20.2		22.0	F0.1 23.0
F1.7 20.7	19.7		21.1	F0.6 22.1
F1.8 22.2	21.2		23.5	C0.9 24.5
F1.4 21.3	20.3		21.1	C0.1 22.1
F1.5 21.5	20.5		21.9	F0.2 22.9
F1.2 22.7	21.7		24.8	E1.2 25.8
F0.5 23.4	22.4		25.0	C1.7 26.0

257	1199.78	2.33
258	1200.10	2.21
259	1200.44	1.87
260	1200.55	4.80
261	1199.85	5.50
262	1198.12	9.23
263	1195.50	9.85
264	1193.13	3.92
265	1191.50	5.55
266	1198.63	6.42
267	1190.50	6.55

B.M. #30
Spike in root 30"
forked Ash. Sta. 261+00
Elev. 1203.18

X Headland
1112.31

F1.1 22.8	21.8		23.5	C0.5 24.5	
F1.5 21.0	20.0		21.1	F0.4 22.1	
F1.9 20.8	19.8		21.7	F0.3 22.7	
F1.0 22.2	21.2		24.8	C1.9 25.8	
C0.9 17.0	16.0		18.5	C2.7 19.5	
F0.1 16.3	15.3		16.0	C1.4 17.0	
C0.1 22.3	21.3		22.1	C0.7 23.1	
C0.6 24.4	23.4		24.5	C1.3 25.5	
C0.4 23.6	22.6		23.4	C1.6 24.4	
F0.6 22.9	21.9		22.0	F0.1 23.0	
F0.7 23.0	22.0		21.9	F0.6 22.9	

268	1190.75	4.61	F1.0 21.5	20.5	20.7	F1.0 21.7
269	1191.00	4.36	F0.9 22.1	21.1	21.0	F0.8 22.0
270	1191.25	4.11	F1.0 21.8	20.8	21.5	F1.0 22.5
271	1191.73	3.63	F0.9 22.0	21.0	21.6	F0.8 22.6
272	1192.66	2.70	F0.8 21.0	20.0	21.2	F0.6 22.2
273	1193.82	1.54	C0.2 21.6	20.6	21.2	C0.4 22.2
274	1194.98	5.27	F0.3 23.1	22.1	22.0	F0.3 23.0
275	1196.15	4.10	C0.0 23.7	22.7	21.6	F0.7 22.6
276	1197.32	2.93	C0.0 23.5	22.5	21.6	F0.4 22.6
277	1198.33	1.92	C0.0 23.2	22.2	21.4	F0.7 22.4

278	1199.00	5.18
279	1199.50	4.68
280	1199.56	4.62
281	1198.75	5.49
282	1197.50	6.74
282+24	1197.20	

1200.24

C0.0				C0.2
23.3	22.3		23.0	24.0
C0.3				C0.5
24.0	23.0		23.1	24.1
C0.4				C0.3
23.6	22.6		23.1	24.1
C1.0				C0.6
24.0	23.0		23.7	24.7
C1.9				C0.9
26.0	25.0		23.0	24.0

Set by Formula

Sta	B.S.	H.I.	F.S.	Rod	BM.25
	3.23	1214.41	3.23		1211.18
221+00		1209.33		5.08	
222+00		1210.00		4.41	
223+00		1210.67		3.74	
224+00		1211.33		3.08	
					1211.18
	3.64	1214.82			
225+00		1211.75		3.04	
226+00		1211.80		3.02	
227+00		1211.60		3.22	

Fo.1 / 23.5	Fo.5 / 22.5	F1.2 / 21.5	F1.1 / 21.5
Fo.5 / 23.5	Fo.5 / 22.5	F1.5 / 22.0	F1.2 / 23.0
C0.0 / 23.4	Fo.6 / 22.4	F1.3 / 21.4	F1.3 / 22.4
C0.8 / 25.0	C0.5 / 24.0	F1.0 / 21.8	Fo.8 / 22.8
C0.4 / 24.4	C0.1 / 23.4	Fo.9 / 22.0	Fo.7 / 23.0
Fo.9 / 22.8	F1.0 / 21.8	F2.4 / 19.7	F2.2 / 20.7
F2.0 / 21.0	F2.3 / 20.0	F3.3 / 20.3	F3.1 / 21.3

Sta	B.S	H.I	F.S	Rod	E.M.Elev
		1214.82			
228+00		1211.40		3.42	
229+00		1211.20		3.62	
			2.23	1212.59	1212.58
	0.26	1212.84			
230+00		1210.63		2.21	
231+00		1209.34		3.50	
232+00		1207.67		5.17	
233+00		1206.42		6.42	
234+00		1206.00		6.84	
			6.00	1206.84	
	4.93	1211.77			
			4.21	1207.56	1207.59

27
23.3

F2.5	F.2.7	F.2.9	F2.9
20.2	19.2	20.4	21.4
F0.5	F0.5	F0.8	F0.6
23.5	22.5	22.1	23.1
C-0.9	C-0.7	C1.0	C1.0
25.4	24.4	24.8	25.8
C-0.1	C-00	F0.8	F0.3
24.5	23.5	22.1	23.1
C-0.5	C-02	C-0.8	C-0.8
24.6	23.6	24.8	25.3
C-1.1	C-0.8	C-1.6	C-1.7
25.5	24.5	25.7	26.7
C-0.9	C-0.7	C-0.9	C-1.0
25.4	24.4	24.6	25.6

Sta	B.S	H I	F.S.	Rod	BM #26 1211.18
	3.01	1214.19			
220+00	1208.67			5.52	
219+00	1207.52			6.67	
218+00	1205.40			8.79	
			7.87	1206.32	
	0.12	1206.44			
217+00	1202.82			3.62	
216+00	1200.24			6.20	
215+00	1197.66			8.78	BM #25
			6.95	1199.49	1199.48
	1.64	1195.34	12.74	1193.70	T.P
214+00	1194.82			0.52	
213+00	1192.20			5.14	

23.3

C 0.8	C 0.7	Fo 0.6	Fo 0.4
25.3	24.3	22.4	23.4
C 1.1	C 0.7	Fo 0.3	Fo 0.1
25.4	24.4	22.8	23.8
C 1.7	C 1.5	C 0.1	C 0.2
26.5	25.5	23.5	24.5
C 1.7	C 1.5	Fo 0.3	Fo 0.2
26.5	25.5	22.8	23.8
C 1.2	C 1.1	Fo 0.3	Fo 0.3
25.9	24.9	22.8	23.8
Fo 0.5	Fo 0.7	F 1.5	F 1.5
23.2	22.2	21.1	22.1
C 0.0	Fo 0.4	F 1.7	F 1.7
23.7	22.7	20.8	21.8
C 1.2	C 1.0	C 0.1	C 0.3
25.8	24.8	23.5	24.3

Sta	B S.	H I	F.S.	Rod	Elev
	1.34	1195.04.		1193.70	T.P.
212+00	1183.52			11.52.	
			12.67	1182.37	T.P.
	0.90	1183.27			
211+00	1175.07.			8.20	
			13.06	1170.21	T.P.
	0.08	1170.29			
210+00	1166.37			3.92	BM #24
			6.22	1164.07	Elev 1164.06
209+00	1157.67			12.62	
			12.76	1157.53	T.P.
	1.48	1159.01			
208+00	1148.97			10.04	
			9.65	1149.36	T.P.

233

C 2.1	C 2.0	C 0.5	C 0.6
27.3	26.3	24.0	25.0
C 2.8	C 2.3	C 2.0	C 2.2
27.8	26.8	26.3	27.3
C 1.4	C 0.9	C 1.4	C 1.7
25.6	24.6	25.4	26.4
C 2.4	C 2.0	C 1.7	C 1.8
27.3	26.3	25.8	26.8
C 4.3	C 4.2	C 3.9	C 4.0
30.6	29.6	29.2	30.2

Set by Formula

Sta	B.S.	H.I	F.S	G Rod	Elev# BM 24 1164.06
	0.22	1164.28			
			1.017	1154.11	T.P
	0.13	1154.24			
207+00	1140.27			13.97	
			12.47	1141.77	T.P
	2.80	1144.57			
206+00	1131.57			13.00	
			13.08	1131.49	T.P
	1.09	1132.58			
205+00	1123.15			9.43	
	0.71	1120.37			
204+00	1114.73			5.64	
			12.81	1107.56	T.P
	1.48	1109.04			
203+00	1106.31			2.73	
202	1097.84			11.15	
			12.03	1097.01	T.P
	1.17	1098.18			
201+00				8.71	

7' Birm Sta 203+00 to Sta 205+00

C 6.8 / 34.2	C 6.7 / 33.2	C 6.6 / 33.2	C 6.6 / 34.3
C 3.7 / 29.8	C 3.7 / 28.8	C 2.8 / 27.5	C 2.9 / 28.5
C 0.1 / 22.5	F 1.9 / 21.5	Spec F 1.2 / 21.5	F 1.5 / 22.5
C 0.0 / 22.9	F 1.6 / 20.9	Spec F 4.1 / 22.1	F 4.1 / 24.1
F 4.8 / 24.4	F 4.8 / 22.4	Spec F 3.1 / 19.9	F 3.2 / 21.9
C 0.4 / 24.9	C 0.4 / 23.9	C 1.1 / 24.9	C 1.2 / 25.9
C 3.7 / 29.9	C 3.7 / 28.9	C 3.1 / 27.9	C 3.3 / 28.9

Sta	B S	H I	F S	G Rod	Elev	
200+00	1081.05			17.13		
			1236	1085.82	T.P.	
	0.65	1086.47		(172)		
199+00	1072.98			13.49		
			1255	1073.92		
	0.78	1074.70				
198+00	1067.32			7.38		
					old BM #23	
			778	1066.92	1066.87	
			11.50	1063.20		
197+00	1064.44					
196+00	1063.98					

C7.0	C6.9	C6.1	C6.2
34.6	33.6	32.4	33.4
C6.2	C5.5	F1.3	F2.2
32.6	31.6	21.4	22.4
F4.3	F4.3	F3.2	F3.0
22.7	21.7	20.1	21.1

Set by Formula

Sta.	B. S	H. I	F. S	G. Rod	BM #22 Elev 1053.09
	10.94	1064.03			
192+00	1062.71			1.32	
191+00	1060.62			3.41	
190+00	1056.94			7.09	
189+00	1053.66			10.37	BM #22
			10.94	1053.09	1053.09
	3.03	1056.12			
188+00					
187+00	1053.36			2.76	
186+00	1057.92			-1.80	

88

66

Special Sections on Curve

F1.2 22.7	F1.1 21.7	F1.2 21.5	F1.1 22.5
F1.8 21.6	F1.8 20.6	F1.1 21.7	F1.2 22.7
E2.2 16.7	15.7		E3.1 26.2
E5.5 21.9	20.9	25.2	E2.7 26.7

Sta. falls on Bridge

F6.5 32.8	31.8	26.6	F5.2 27.6
10.2 40.4	39.4	30.2	F6.7 31.2

Sta	B.S.	H.I	F.S.	G Rod	Elev
185+50	1061.36			-5.24	BM #21
			1.59	1054.53	1054.56
	10.69	1065.25			
			2.49	1062.76	T.P
	12.06	1074.82			
185+00	1065.59			9.23	
			2.20	1072.62	T.P
	12.98	1085.60			
184+00	1074.84			10.76	
			1.03	1084.57	T.P
	10.93	1095.50			
183+00	1084.08			11.42	
182+00	1093.33			2.17	
			0.50	1095.00	T.P
	11.68	1106.68			
181+00	1102.57			4.11	

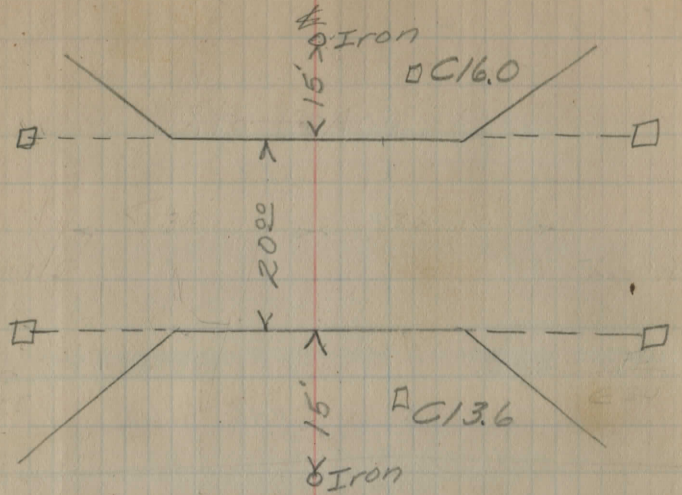
Special on Curve

Right		Left	
F6.7			F8.7
33.6	32.6	38.8	39.8
C6.1			Fa2
35.7	34.7	20.3	21.3
C6.0			E4.0
35.4	34.4	27.0	28.0
F1.5	F1.6	C4.7	C4.7
21.9	20.9	30.3	31.3
F1.7	F1.5	E1.5	C1.7
22.1	21.1	25.5	26.5
F.4.4			F.4.7
27.1	26.1	25.6	26.6

8/12/28 Richey Parks Spohn

BM	5.00	1058.09			1053.09
Flow			2.036		1037.73
Stake S				6.76	C13.6
Stake N				4.36	C16.0

Sta 187+92



BM #20

Set by Formula

Elev 1116.69

Sta.	B.S.	H.I.	F.S.	G. Rod.	
	0.22	1116.91			
			12.54	1104.37	
	3.47	1107.84			
180+00	1111.82			- 3.98	
+50	1116.44			- 8.60	
			0.96	1106.88	T.P.
	12.76	1119.64			
179+00	1121.06			- 1.42	
			2.95	1116.69	B.M. chk.
	12.98	1129.67			
178+50	1125.68			3.99	
			1.66	1128.01	T.P.
	12.95	1140.96			
178+00	1130.81			10.65	
			0.56	1140.40	T.P.
	5.99	1146.39			
177+50	1134.94			11.45	
			1.33	1145.06	T.P.
	5.14	1150.20			
177+00	1139.57			10.63	

F11.1 / 40.0 | F11.9 / 39.0

F9.5 / 39.8 | — / 38.8

F7.1 / 32.4 | 5.8 / 31.4

F1.4 / 24.3 | 6.0 / 23.3

C5.3 / 35.0 | 5.5 / 34.0

C5.7 / 25.8 | 5.2 / 24.8

C7.2 / 26.0 | 3.9 / 25.0

F12.1 / 40.4 | F12.0 / 41.4

— / 39.2 | F11.6 / 40.2

4.9 / 28.9 | F6.1 / 29.9

6.0 / 20.0 | F1.7 / 21.0

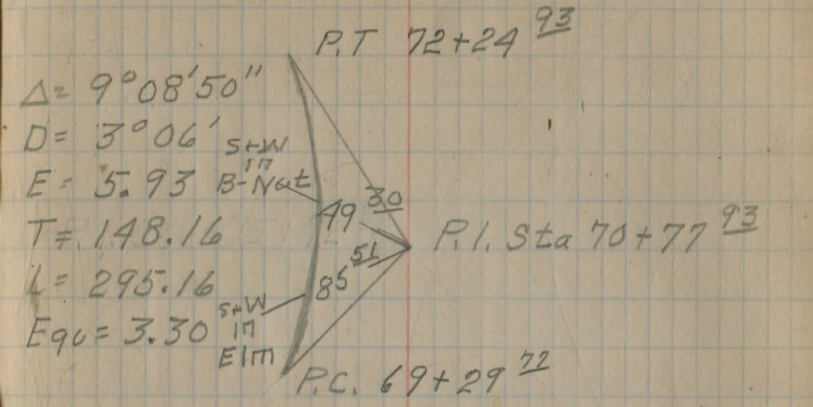
— / 26.0 | C1.4 / 27.0

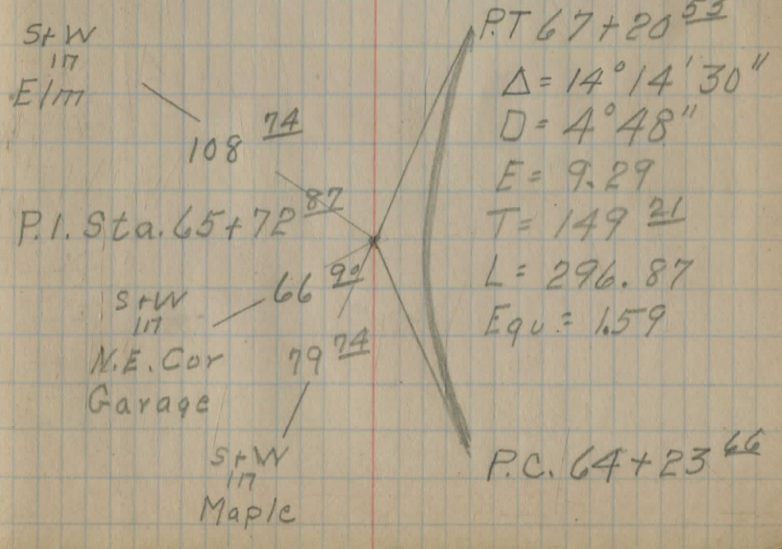
12.0 / 20.9 | C0.5 / 21.9

C1.2 / 23.1 | C2.5 / 24.1

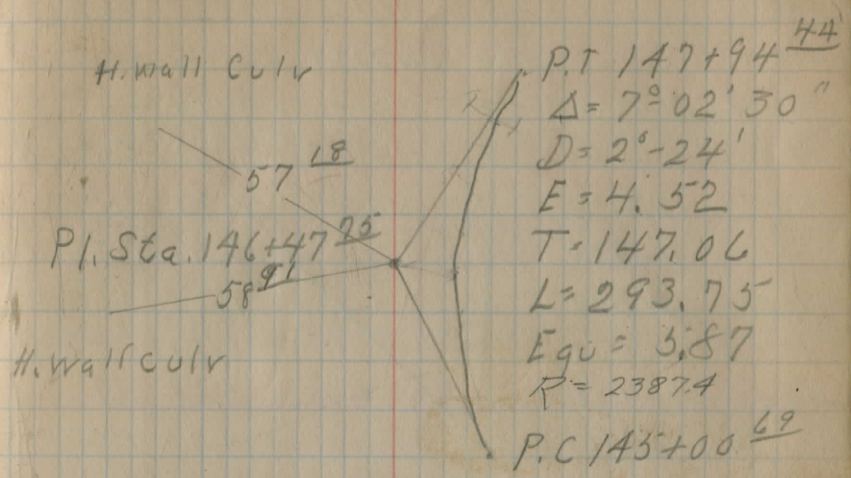
Sta	B.S.	H.I	F.S.	G. Rod	
176+50	1144.19			6.01	B.M. #19
			0.82	1149.38	1149.36
	12.60	1161.96			
176+00	1148.82			13.14	
+50	1153.45			8.51	
			0.96	1161.00	T.P.
	11.80	1172.80			
175+00	1158.08			14.72	
+50	1162.70			10.10	
			1.12	1171.68	T.P.
	8.15	1179.83			
174+00	1167.33			12.50	B.M. 18
			2.01	1177.82	1177.83
+50	1171.95			7.88	
	8.00	1185.83			
173+00	1176.58			9.25	

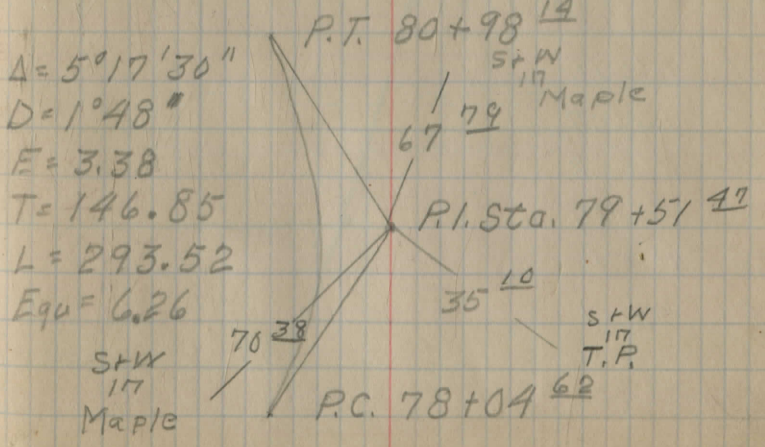
C3.1		C25	C2.9
22.7	21.7	23.1	24.1
C6.5	7.3		C1.8
25.5	24.5	21.9	22.9
C7.3	1.7	1.6	C7.0
26.0	25.0	27.2	28.2
C6.9	7.8	8.2	C6.8
25.0	24.0	27.2	28.2
C5.5	5.0	4.2	C6.1
22.9	21.9	28.8	29.8
C3.2	10.2	6.9	C6.0
21.2	20.2	30.3	31.3
C1.7	6.7	3.7	C4.2
20.8	19.8	29.1	30.1
C0.0	9.4	4.9	C4.6
20.4	19.4	29.2	30.2


P.T 72+24 93
Δ = 9°08'50"
D = 3°06'
E = 5.93
T = 148.16
L = 295.16
Equ = 3.30
S+W in B-Nut
S+W in Elm
49 30
51
85
P.I. Sta 70+77 93
P.C. 69+29 72


S+W in Elm
108 74
P.I. Sta. 65+72 87
S+W in N.E. Cor Garage
66 90
79 74
S+W in Maple
P.T 67+20 53
Δ = 14°14'30"
D = 4°48"
E = 9.29
T = 149 21
L = 296.87
Equ = 1.59
P.C. 64+23 66

3.38
1°-48


H. wall Culv
57 18
Pl. Sta. 146+47 25
58 81
H. wall culv
P.T 147+94 44
Δ = 7°02'30"
D = 2°-24'
E = 4.52
T = 147.06
L = 293.75
Equ = 5.87
R = 2387.4
P.C 145+00 69


Δ = 5°17'30"
D = 1°48"
E = 3.38
T = 146.85
L = 293.52
Equ = 6.26
P.T. 80+98 14
St+W 17 Maple
67 79
Pl. Sta. 79+51 47
35 10
St+W 17 T.P.
70 38
St+W 17 Maple
P.C. 78+04 62

BM # 0+00
Elev 1045.55

Sta		B.S	H.I.	F.S	
		11.69	1057.24		
0+00	1047.50			9.74	L
+50	1048.11			9.13	Cut 1.0
1+00	1048.72			8.52	Cut 0.5
+50	1049.33			7.91	Cut 0.5
2+00	1049.99			7.25	" 0.5
+50	1050.73			6.51	" 0.5
3+00	1051.58			5.66	Cut 1.0
+50	1052.51			4.73	L
4+00	1053.50			3.74	Cut 1.0
+50	1054.69			2.59	Cut 1.5
5+00	1055.82				
+50	1057.16				
6+00	1058.55				
+50	1060.02				
7+00	1061.60				
+50	1062.26				
8+00	1064.97				
+50	1066.68				
9+00	1068.39				
+50	1070.10				
10+00	1071.81				

1045.55
11.69
1057.24

BM # Sta 10+50
Elev. 1075.48

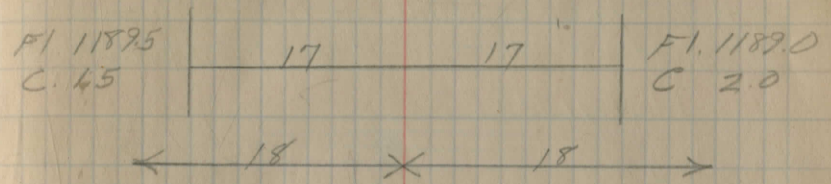
BM #17	4.05	1196.30			1192.25
Flow R			7.30	1189.00	
Stake R			5.30		C 2.0
Flow L			6.80	1189.50	
stake L			5.30		C 1.5

BM 21	3.37	1057.93			1054.56
Flow S			10.63	1047.30	
stake S			9.1	C 1.5	
Flow N			11.13	1046.80	
stake N			9.63	C 1.5	

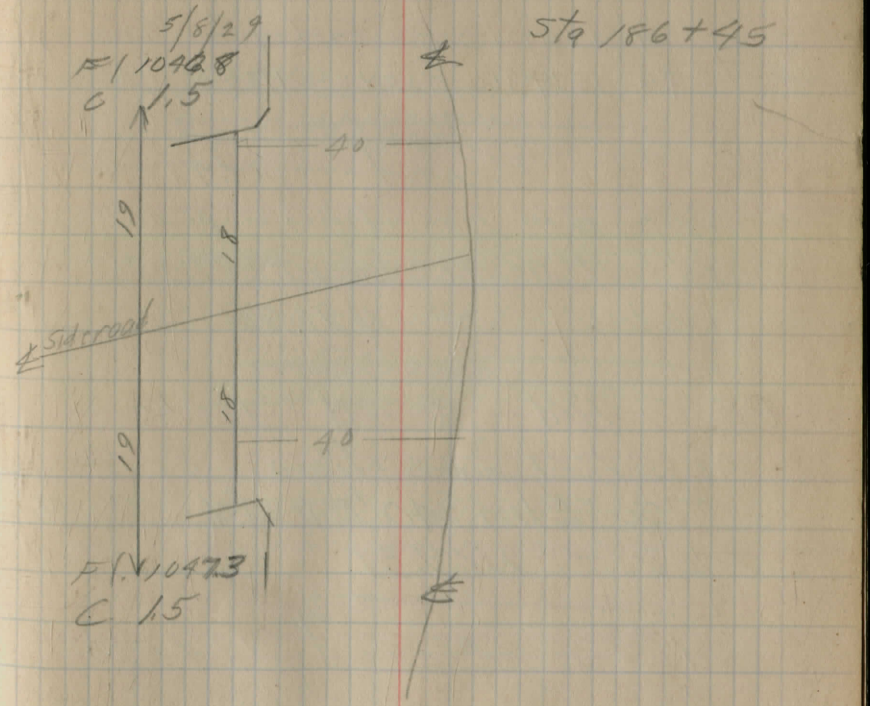
5/8/29 Richey Grundy Rand Ashcroft

74

18" VSD Sta 164+75



Sta 186+45



BM #15 Moved 134+06
New bench Located on root of
40" Maple 30' East of ℄ Sta 134+06
Elev 1153.85

BM #11 Moved 103+36
New bench Location - Spike in root
of 24" Maple 100' East of ℄
Sta 103+36 Elev = 1126.00

BM #31 Moved 268+04
New BM Location - NW ℄ West
Headwall new culvert Sta 268+04
Elev - 1191.05

USGS-BM Moved 145+00
New BM Location Spike in
root 30" Elm 40' Rt of ℄ Sta 145+00
Elev - 1169.31

BM #23 Moved 197+80
New BM Location Spike
in root Maple 35' Lt of ℄ Sta 197+80
Elev. - 1063.32

BM #29 Moved 248+30
New BM Location Spike in
root 24" Maple 30' E of ℄
Sta 248+30
Elev - 1203.26

BM #20 Moved 179+10
New BM Location Spike in
root Twin 15" Ash 50' E of ℄
Sta 179+10
Elev - 1113.83

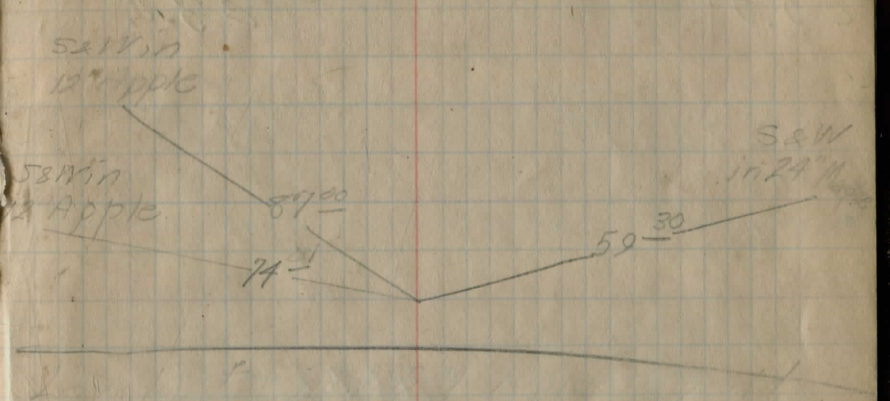
BM #3 Moved 21+45
New BM Location Spike in
root 18" Elm 30' Lt of ℄ Sta 21+45
Elev - 1109.76

BM #7 Moved 66+80
New BM Location Spike in
root 30" Elm 35' Lt of ℄ Sta 66+80
Elev - 1054.53

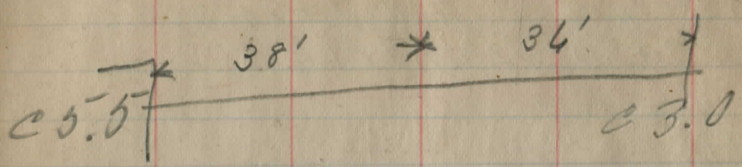
Levels for New US65 BM replacing old US65 BM at Sta 47+08

	BS	HI	FS	Elev
Temp BM	2.43	1171.74		1169.31
New BM			5.33	1166.41
New BM	4.70	1171.11		1166.41
Temp BM			1.80	1169.31

References to Iron Pipe at Sta 53+83 26' Rt of ℄ ±



Culverts



FL 1097.5 1096.5

17745

8 8-52

1101.5 G

B.M. 1116.69
0.27
1116.96+
10.78
1106.18
1.14
1107.32

1107.32
6.40
1100.92

1107.32
1097.5
9.8
4.3
5.5

1007.3
1096.5
10.8
7.8
3.0

1.70
1169.31
1171.01

Flow 7.5

NW 352
NE 317
SE 356
SW 349

3-29
4-15
7-44
4 15 204
11-59
4 15
16 14
2 09
18 23

5.1
41
51
2091
40
5.1
207.0

1163.86
2.12
1165.98

3-24

8 30 = 100
4 15 50

5 1/ = 1

25.4
5.1
25.4
127
129

IMPROVED TABLES

AND

INFORMATION

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1½ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

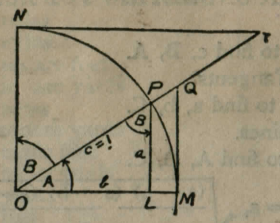


TABLE II

TRIGONOMETRIC FORMULÆ.

$\angle A = \angle MOP \qquad \angle B = \angle PON = \angle OPL$

$R = OB = c = 1$

$$\sin A = \frac{a}{c} = \frac{a}{1} = a = \cos B = LP$$

$$\cos A = \frac{b}{c} = \frac{b}{1} = b = \sin B = OL$$

$$\tan A = \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ$$

$$\cot A = \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT$$

$$\sec A = \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ$$

$$\csc A = \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT$$

$$\text{vers } A = \frac{LM}{OP} = LM = \text{covers } B \#$$

$$\text{covers } A = \frac{OP - LP}{OP} = OP - LP = \text{vers } B$$

$$\text{exsec } A = PQ = \text{coexsec } B$$

$$\text{coexsec } A = PT = \text{exsec } B$$

$$\sin \tfrac{1}{2} A = \sqrt{\frac{1 - \cos A}{2}} \qquad \cos \tfrac{1}{2} A = \sqrt{\frac{1 + \cos A}{2}}$$

$$\sin 2A = 2 \sin A \cos A \qquad \cos 2A = \cos^2 A - \sin^2 A$$

Law of Sines $\dfrac{\sin A}{a} = \dfrac{\sin B}{B} = \dfrac{\sin C}{C}$

Law of Cosines $c^2 = a^2 + b^2 - 2ab \cos C$

Law of Tangents $\dfrac{a+b}{a-b} = \dfrac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)}$

Table II—Continued
TRIGONOMETRIC FORMULAE (continued)

In any triangle:

Given a, b, C; to find c, B, A.

Use Law of Tangents.

Given A. B. c; to find a, b, C.

Use Law of Sines.

Given a, b, c; to find A, B, C.

$$\text{Let } \frac{a+b+c}{2} = s, \sqrt{\frac{(s-a)\,(s-b)\,(s-c)}{s}} = r$$

$$\cos \tfrac{1}{2} A = \sqrt{\frac{s(s-a)}{bc}}$$

$$\tan \tfrac{1}{2} A = \frac{r}{s-a}$$

$$\tan \tfrac{1}{2} B = \frac{r}{s-b}$$

$$\tan \tfrac{1}{2} C = \frac{r}{s-c}$$

Area of a triangle:

Area $= \tfrac{1}{2}$ ab Sin C

Area $= \sqrt{s\,(s-a)\,(s-b)\,(s-c)}$

PRISMOIDAL FORMULA.

$$\text{Vol.} = \frac{h}{6}(B+b+4M)$$

h = altitude: b B = bases; M = midsection

Table III
INCHES AND FRACTIONS OF AN INCH IN DECIMALS OF A FOOT

	0	1	2	3	4	5	6	7	8	9	10	11	
1	.0052	.0885	.1719	.2552	3385	4219	.5052	5885	.6719	.7552	.8385	9219	1
1/16	.0104	.0938	.1771	.2604	.3438	.4271	.5104	.5938	.6771	.7604	.8438	.9271	1/16
1/8	.0156	.0990	.1823	.2656	.3490	.4323	.5156	.5990	.6823	.7656	.8490	.9323	1/8
3/16	.0208	.1042	.1875	.2708	.3542	.4375	.5208	.6042	.6875	.7708	.8542	.9375	3/16
1/4	.0260	.1094	.1927	.2760	.3594	.4427	.5260	.6094	.6927	.7760	.8594	.9427	1/4
5/16	.0313	.1146	.1979	.2813	.3646	.4479	.5313	.6146	.6979	.7813	.8646	9479	5/16
3/8	.0365	.1198	.2031	.2865	.3698	.4531	.5365	.6198	.7031	.7865	.8698	.9531	3/8
7/16	.0417	.1250	.2083	.2917	.3750	.4583	.5417	.6250	.7083	.7917	.8750	.9583	7/16
1/2	.0469	.1302	.2135	.2969	.3803	.4635	.5469	.6302	.7135	.7969	.8802	.9635	1/2
9/16	.0521	.1354	.2188	.3021	.3854	.4688	.5521	.6354	.7188	.8021	.8854	9688	9/16
5/8	.0573	.1406	.2240	.3073	.3906	.4740	.5573	.6406	.7240	.8073	.8906	.9740	5/8
11/16	.0625	.1458	.2292	.3125	.3958	.4792	.5625	.6458	.7292	.8125	.8958	.9792	11/16
3/4	.0677	.1510	.2344	.3177	.4010	.4844	.5677	.6510	.7344	.8177	.9010	.9844	3/4
13/16	.0729	.1563	.2396	.3229	4063	.4896	.5729	.6563	.7396	.8229	.9063	9896	13/16
7/8	.0781	.1615	.2448	.3281	.4115	4948	.5781	.6615	.7448	.8281	.9115	.9948	7/8
15/16	.0833	.1667	.2500	.3333	.4167	.5000	.5833	.6667	.7500	.8333	.9167	1.000	15/16
1	0	1	2	3	4	5	6	7	8	9	10	11	1

Table IV
USEFUL RELATIONS.

Lineal feet	×.00019	= miles
Lineal yards	×.0006	= miles
Square inches	×.007	= square feet
Square feet	×.111	= square yards
Square yards	×.0002067	= acres
Acres	×4840	= square yards
Cubic inches	×.00058	= cubic feet
Cubic feet	×.03704	= cubic yards
Links	×.22	= yards
Links	×.66	= feet
Feet	×1.5	= links

360° = 21600′ = 1296000″

Radius = arc of 57.2957790°

Arc of 1° (radius = 1) = .017453292

Arc of 1′ (radius = 1) = .000290888

Arc of 1″ (radius = 1) = .000004848

$\pi = 3.141592654$ $\qquad \sqrt{\frac{1}{4}} = 0.564190$

$\frac{\pi}{4} = 0.785398163$ $\qquad \sqrt[3]{\frac{6}{\pi}} = 1.240700982$

$\frac{\pi}{6} = 0.523598776$ $\qquad \pi^2 = 9.869604401$

$\sqrt{\frac{4}{\pi}} = 1.128379167$ $\qquad \frac{1}{\pi^2} = 0.101321184$

$\frac{\pi}{6} = 0.523598776$ $\qquad \sqrt{\pi} = 1.772453851$

$\frac{4.\pi}{3} = 4.188790205$ $\qquad \frac{1}{\pi} = 0.3183099$

Curvature of Earth's surface = about 0.7 feet in 1 mile

Curvature in feet = 0.667 (Dist. in miles)^2

Difference between arc and chord length, 0.05 feet in 11½ miles

Probable error of a single observation $= 0.6754\sqrt{\frac{\Sigma v^2}{n-1}}$

Error in chaining of 0.01 feet in 100 feet:

Due to—

1. Length of tape error of 0.01 feet
2. Alignment. One end 1.4 feet out of line
3. Sag of tape at centre of 0.61 feet.
4. Temperature difference of 15°
5. Difference of pull of 15 lbs.

STADIA REDUCTION FORMULÆ.

Horizontal Distance $= R - R \sin^2 a + C \cos a$

Vertical Distance $= R \tfrac{1}{2} \sin 2a + C \sin a$

$R = \text{Reading} \times \frac{\text{distance from Object glass to cross hairs}}{\text{distance between cross hairs}}$

C = distance from Object glass to cross hairs + distance from Object glass to center of instrument.

a = angle of elevation for mid Reading

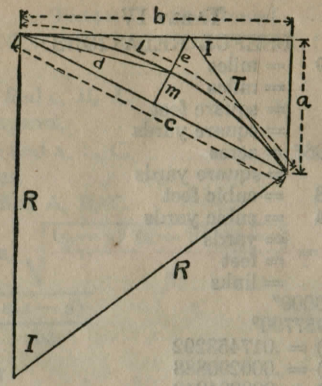


Table V

CURVE FORMULAE FOR SIMPLE CURVES

Compiled by J. Calvin Locke, C.E.

(1) $c = \sqrt{2Ra}$ (2) $c = \sqrt{a^2+b^2}$

(3) $c = \sqrt{2R\,(R-\sqrt{(R+b)\,(R-b)}} = \sqrt{2R(R-\sqrt{R^2-b^2})}$

(4) $c = 2\sqrt{m\,(2R-m)}$

(5) $c = 2R \sin \frac{1}{2} I$ (6) $c = 2T \cos \frac{1}{2} I$

(7) $e = R \operatorname{exsec} \frac{1}{2} I$

(8) $e = R \tan \frac{1}{2} I \tan \frac{1}{4} I$ (9) $e = T \tan \frac{1}{4} I$

(10) $b = \sqrt{a\,(2R-a)}$

(11) $b = \sqrt{\left(c+\frac{c^2}{2R}\right)\left(c-\frac{c^2}{2R}\right)} = \sqrt{c^2-\frac{c^4}{4R^2}}$

(12) $b = R \sin I$ (13) $b = a \cot \frac{1}{2} I$

(14) $R = \frac{a^2+b^2}{2a} = \frac{c^2}{2a}$ (15) $R = \frac{d^2}{2m} = \frac{c^2+4m^2}{8m}$

(16) $d = \sqrt{R\,(2R-\sqrt{(2R+c)\,(2R-c)}} = \sqrt{R(2R-\sqrt{4R^2-c^2})}$

(17) $d = \sqrt{2Rm}$ (18) $d = 2R \sin \frac{1}{4} I$ (19) $m = \frac{d^2}{2R}$

(20) $m = R \mp \sqrt{\left(R+\frac{c}{2}\right)\left(R-\frac{c}{2}\right)} = R \mp \sqrt{R^2-\frac{c^2}{4}}$

(21) $m = R \operatorname{vers} \frac{1}{2} I$ (22) $m = R \sin \frac{1}{2} I \tan \frac{1}{4} I$ (23) $m = \frac{1}{2} c \tan \frac{1}{4} I$

(24) $a = \frac{c^2}{2R}$ (25) $a = R - \sqrt{(R+b)\,(R-b)} = R - \sqrt{R^2-b^2}$

(26) $a = 2R\,(\sin^2 \frac{1}{2} I)^2$ (27) $a = R \operatorname{vers} I$ (28) $a = R \sin I \tan \frac{1}{2}$

(29) $a = b \tan \frac{1}{2} I$ (30) $a = T \sin I$ (31) $T = R \tan \frac{1}{2} I$

(32) $I = \frac{L}{R} \times 57.295780$ (33) $R = \frac{L}{I} \times 57.295780$

(34) $L = IR \times 0.01745329$ (35) $L = \frac{8d-c}{3}$

(36) Area Seg. $= \frac{LR - R^2 \operatorname{Sin} I}{2} = \frac{LR - Rb}{2}$

Table VI

SINES, COSINES, TANGENTS, COTANGENTS

deg.	sin 0′	tan 0′	sin 10′	tan 10′	sin 20′	tan 20′	sin 30′	tan 30′	sin 40′	tan 40′	sin 50′	tan 50′	deg.
0	0000	0000	0029	0029	0058	0058	0087	0087	0116	0116	0145	0145	89
1	175	0375	0204	0204	0233	0233	0262	262	291	291	320	320	88
2	349	349	378	378	407	407	436	437	465	466	494	495	87
3	523	524	552	553	581	582	610	612	640	641	669	706	86
4	698	699	727	729	756	758	785	787	814	816	843	864	85
5	872	875	901	904	929	934	958	963	987	992	1016	1022	84
6	1045	1051	1074	1080	1103	1110	1132	1139	1161	1169	190	198	83
7	219	228	248	257	279	287	305	317	334	346	363	376	82
8	392	405	421	435	449	465	478	495	507	524	536	554	81
9	564	584	593	614	622	644	650	673	679	703	708	733	80
10	736	763	765	793	794	823	822	853	851	883	880	914	79
11	908	944	937	974	965	2004	994	2035	2022	2065	2051	2095	78
12	2079	2126	2108	2156	2136	186	2164	217	193	247	221	278	77
13	250	309	278	339	306	370	334	401	363	432	391	462	76
14	419	493	447	524	476	555	504	586	532	617	560	648	75
15	588	679	616	711	644	742	672	773	700	805	728	836	74
16	756	867	784	899	812	931	840	962	868	994	896	3026	73
17	924	3057	952	3089	939	3121	3007	3153	3035	3185	3062	217	72
18	3090	249	3118	281	3145	314	173	346	201	378	228	411	71
19	256	443	283	476	311	508	338	541	365	574	393	607	70
20	420	640	448	673	475	706	502	739	529	772	557	805	69
21	584	839	611	872	638	906	665	939	692	973	719	4006	68
22	746	4040	773	4074	800	4108	827	4142	854	4176	881	210	67
23	907	245	934	279	961	314	987	348	4014	383	4041	417	66
24	4067	452	4094	487	4120	522	4147	557	173	592	200	628	65
25	226	663	253	699	279	734	305	770	331	806	358	841	64
26	384	877	410	913	436	950	4462	986	488	5022	514	5059	63
27	540	5095	566	5132	592	5169	617	5206	643	243	669	280	62
28	695	317	720	354	746	392	772	430	797	467	823	505	61
29	848	543	874	581	899	619	924	658	950	696	975	735	60
30	5000	774	5025	5812	5050	851	5075	890	5100	930	5125	969	59
31	150	6009	175	6048	200	6088	225	6128	250	6168	275	6208	58
32	299	249	324	289	348	330	5373	371	398	412	422	453	57
33	446	494	471	536	495	577	519	619	544	661	568	703	56
34	592	745	616	787	640	830	664	873	688	916	712	959	55
35	736	7002	760	7046	783	7089	807	7133	831	7177	854	7221	54
36	878	265	901	310	925	355	948	400	972	445	995	490	53
37	6018	536	6041	581	6065	627	6088	673	6111	720	6134	766	52
38	157	813	180	860	202	907	225	954	248	8002	271	8050	51
39	293	8098	316	8146	338	8195	361	8243	383	292	406	342	50
40	428	391	450	441	472	491	494	541	517	591	539	642	49
41	561	693	583	744	604	796	626	847	648	899	670	952	48
42	691	9004	713	9057	734	9110	756	9163	777	9217	799	9271	47
43	820	325	841	380	862	435	884	490	905	545	926	601	46
44	947	657	967	713	988	770	7009	827	7030	884	7050	942	45
45	7071	1.0000	7092	1.0058	7112	1.0117	133	1.0176	153	1.0235	173	1.0295	44
deg.	60′ cos	60′ cot	50′ cos	50′ cot	40′ cos	40′ cot	30′ cos	30′ cot	20′ cos	20′ cot	10′ cos	10′ cot	deg.

TABLE VI (continued)

SINES, COSINES, TANGENTS, COTANGENTS (continued)

deg.	sin 0′	tan 0′	sin 10′	tan 10′	sin 20′	tan 20′	sin 30′	tan 30′	sin 40′	tan 40′	sin 50′	tan 50′	deg.
46	7193	1.0355	7214	1.0416	7234	1.0477	7254	1.0533	7274	1.0599	7294	1.0661	43
47	314	.0724	333	.0786	353	.0850	373	.0913	392	.0977	412	.1041	42
48	431	.1106	451	.1171	470	.1237	490	.1303	509	.1369	528	.1436	41
49	547	.1504	566	.1571	585	.1640	604	.1708	623	.1778	642	.1847	40
50	660	1.1918	7679	1.1988	7698	1.2059	7716	1.2131	7735	1.2203	7753	1.2276	39
51	771	.2349	790	.2423	808	.2497	826	.2572	844	.2647	862	.2723	38
52	880	.2799	898	.2876	916	.2954	934	.3032	951	.3111	969	.3190	37
53	986	.3270	8004	.3351	8021	.3452	8039	.3514	8056	.3597	8073	.3680	36
54	8090	.3764	107	.3848	124	.3934	141	.4019	158	.4106	175	.4193	35
55	192	.4231	208	.4370	225	.4460	241	.4550	258	.4641	274	.4733	34
56	290	.4826	307	.4919	323	.5013	339	.5108	355	5204	371	.5301	33
57	387	.5399	403	.5497	418	.5597	434	.5697	450	5798	465	.5900	32
58	480	.6003	496	.6107	511	.6212	526	.6319	542	.6426	557	.6534	31
59	572	.6643	587	.6753	601	.6864	616	.6977	631	.7090	646	.7205	30
60	660	1.7321	8675	1.7437	8689	1.7556	8704	1.7675	8718	1.7797	8732	1.7917	29
61	746	.8040	760	.8165	774	.8291	788	.8418	802	.8546	816	.8676	28
62	829	.8807	843	.8940	857	.9074	870	.9210	884	.9347	897	.9486	27
63	910	.9626	923	.9768	936	.9912	949	2.0057	962	2.0204	975	2.0353	26
64	988	2.0503	9001	2 0655	9013	2 .0809	9026	.0965	9038	.1123	9051	.1283	25
65	9063	.1445	075	.1609	088	.1775	100	.1943	112	.2113	124	.2286	24
66	135	.2460	147	.2637	159	.2817	171	.2998	182	3183	194	.3369	23
67	205	.3559	216	.3750	228	.3945	239	.4142	250	.4342	261	.4545	22
68	272	.4751	283	.4960	293	.5172	304	.5386	315	.5605	325	.5826	21
69	336	.6051	346	.6279	356	.6511	367	.6746	377	.6985	387	.7228	20
70	397	2.7475	9407	2.7725	9417	2. 7980	9426	2.8239	9436	2.8502	9446	2.8770	19
71	455	.9042	465	.9319	474	. 9600	483	.9887	492	3.0178	502	3.0475	18
72	511	3.0777	520	3.1084	528	3.1397	537	3.1716	546	.2041	555	.2371	17
73	563	.2709	572	.3052	580	.3402	588	.3759	596	.4124	605	.4495	16
74	613	.4874	621	.5261	628	.5656	636	.6059	644	.6470	652	.6891	15
75	659	.7321	667	.7760	674	.8208	681	.8657	689	.9136	696	.9617	14
76	703	4.0108	710	4.0611	717	4 .1126	724	4.1653	730	4.2193	737	4.2747	13
77	744	.3315	750	.3897	757	.4494	763	.5107	769	.5736	775	.6382	12
78	781	.7046	787	.7729	793	.8430	799	.9152	805	.9894	811	5.0658	11
79	816	.1446	822	5.2257	827	5. 3093	833	5.3955	838	5.4845	843	.5764	10
80	9848	5.6713	9853	5.7694	9858	5. 8708	9863	5.9758	9868	6.0844	9872	6.1970	9
81	877	6.3138	881	6.4348	886	6. 5606	890	6.6912	894	.8269	899	.9682	8
82	903	7.1154	907	7.2687	911	7.4287	914	7.5958	918	7.7704	922	7.9530	7
83	925	8.1443	929	8.3450	932	8.5555	936	8.7769	939	9.0098	942	9.2553	6
84	945	9.5144	948	9.7882	951	10.078	954	10.385	957	10.711	959	11.059	5
85	962	11.430	964	11.826	967	12.250	969	12.706	971	13.197	974	13.727	4
86	976	14.300	978	14.924	980	15.605	981	16.350	983	17.169	985	18.075	3
87	986	19.081	988	20.206	989	21.470	990	22.903	992	24.542	993	26.432	2
88	994	28.636	9995	31.242	9996	34.368	997	38.189	997	42.964	9998	49.104	1
89	9998	57.290	9999	68.750	9999	85.940	9999	114.58	1.000	171.88	1.000	343.77	0
deg.	60′ cos	60′ cot	50′ cos	50′ cot	40′ cos	40′ cot	30′ cos	30′ cot	20′ cos	30′ cot	10′ cos	10′ cot	deg.

TABLE VII

RODS IN FEET AND INCHES

Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches
1	16—6	21	346—6	41	676—6	61	1006—6	81	1336—6
2	33—0	22	363—0	42	693—0	62	1023—0	82	1353—0
3	49—6	23	379—6	43	709—6	63	1039—6	83	1369—6
4	66—0	24	396—0	44	726—0	64	1056—0	84	1386—0
5	82—6	25	412—6	45	742—6	65	1072—6	85	1402—6
6	99—0	26	429—0	46	759—0	66	1089—0	86	1419—0
7	115—6	27	445—6	47	775—6	67	1105—6	87	1435—6
8	132—0	28	462—0	48	792—0	68	1122—0	88	1452—0
9	148—6	29	478—6	49	808—6	69	1138—6	89	1468—6
10	165—0	30	495—0	50	825—0	70	1155—0	90	1485—0
11	181—6	31	511—6	51	841—6	71	1171—6	91	1501—6
12	198—0	32	528—0	52	858—0	72	1188—0	92	1518—0
13	214—6	33	544—6	53	874—6	73	1204—6	93	1534—6
14	231—0	34	561—0	54	891—0	74	1221—0	94	1551—0
15	247—6	35	577—6	55	907—6	75	1237—6	95	1567—6
16	264—0	36	594—0	56	924—0	76	1254—0	96	1584—0
17	280—6	37	610—6	57	940—6	77	1270—6	97	1600—6
18	297—0	38	627—0	58	957—0	78	1287—0	98	1617—0
19	313—6	39	643—6	59	973—6	79	1303—6	99	1633—6
20	330—0	40	660—0	60	990—0	80	1320—0	100	1650—0

TABLE VIII

LINKS IN FEET AND INCHES

Links	Feet Inches	Links	Feet Inches	Links	Feet Inches	Links	Feet Inches	Links	Feet Inches	Links	Feet Inches
1	0- 7.92	18	11-10.56	35	23- 1.20	52	34- 3 84	69	45- 6 48	86	56- 9 12
2	1- 3.84	19	12- 6.48	36	23- 9.12	53	34-11.76	70	46- 2 40	87	57- 5 04
3	1-11.76	20	13- 2.40	37	24- 5.04	54	35- 7 68	71	46-10 32	88	58- 0 96
4	2- 7.68	21	13-10.32	38	25- 0.96	55	36- 3 60	72	47- 6.24	89	58- 8.88
5	3- 3.60	22	14- 6.24	39	25- 8.88	56	36-11 52	73	48- 2 16	90	59- 4 80
6	3-11.52	23	15- 2.16	40	26- 4.80	57	37- 7.44	74	48-10 08	91	60- 0 72
7	4- 7.44	24	15-10.08	41	27- 0.72	58	38- 3 36	75	49- 6.00	92	60- 8 64
8	5- 3.36	25	16- 6.00	42	27- 8.64	59	38-11 28	76	50- 1.92	93	61- 4 56
9	5-11.28	26	17- 1.92	43	28- 4.56	60	39- 7 20	77	50- 9.84	94	62- 0 48
10	6- 7.20	27	17- 9.84	44	29- 0.48	61	40- 3 12	78	51- 5.76	95	62- 8 40
11	7- 3.12	28	18- 5 76	45	29- 8.40	62	40-11 04	79	52- 1.68	96	63- 4 32
12	7-11.04	29	19- 1 68	46	30- 4.32	63	41- 6.96	80	52- 9.60	97	64- 0 24
13	8- 6.96	30	19- 9.60	47	31- 0.24	64	42- 2.88	81	53- 5.52	98	64- 8.16
14	9- 2.88	31	20- 5.52	48	31- 8.16	65	42-10.80	82	54- 1.44	99	65- 4.08
15	9-10.80	32	21- 1 44	49	32- 4.08	66	43- 6.72	83	54- 9.36	100	66- .000
16	10- 6.72	33	21- 9.36	50	33- 0.00	67	44- 2.64	84	55- 5.28	101	66 -7.92
17	11- 2.64	34	22- 5.28	51	33- 7.92	68	44-10.56	85	56- 1.20	102	67- 3.84

TABLE IX. TANGENTS AND EXTERNALS TO A 1° CURVE

I	T	E	I=10°	I	T	E	I=20°	I	T	E	I=30°
1°	50.00	.218	+	11°	551.70	26.500	+	21°	1061.9	97.577	+
10′	58.34	.297	5° C.	10′	560.11	27.313	5° C	10′	1070.6	99.155	5° C
20′	66.67	.388	T	20′	568.53	28.137	T	20′	1079.2	100.75	T
30′	75.01	.491	.03	30′	576.95	28.974	.06	30′	1087.8	102.35	.10
40′	83.34	.606	E	40′	585.36	29.824	E	40′	1096.4	103.97	E
50′	91.68	.733		50′	593.79	30.686		50′	1105.1	105.60	
2°	100.01	.873	.001	12°	602.21	31.561	.006	22°	1113.7	107.24	.013
10′	108.35	1.024		10′	610.64	32.447		10′	1122.4	108.90	
20′	116.68	1.188		20′	619.07	33.347		20′	1131.0	110.57	
30′	125.02	1.364		30′	627.50	34.259		30′	1139.7	112.25	
40′	133.36	1.552		40′	635.93	35.183		40′	1148.4	113.95	
50′	141.70	1.752		50′	644.37	36.120		50′	1157.0	115.66	
3°	150.04	1.964	10° C.	13°	652.81	37.070	10° C.	23°	1165.7	117.38	10° C.
10′	158.38	2.188	T	10′	661.25	38.031	T	10′	1174.4	119.12	T
20′	166.72	2.425	.06	20′	669.70	39.006	.13	20′	1183.1	120.87	.19
30′	175.06	2.674	E	30′	678.15	39.993	E	30′	1191.8	122.63	E
40′	183.40	2.934	.003	40′	686.60	40.992	.011	40′	1200.5	124.41	.025
50′	191.74	3.207		50′	695.06	42.004		50′	1209.2	126.20	
4°	200.08	3.492		14°	703.51	43.029		24°	1217.9	128.00	
10′	208.43	3.790		10′	711.97	44.066		10′	1226.6	129.82	
20′	216.77	4.099		20′	720.44	45.116		20′	1235.3	131.65	
30′	225.12	4.421		30′	728.90	46.178		30′	1244.0	133.50	
40′	233.47	4.755		40′	737.37	47.253		40′	1252.8	135.35	
50′	241.81	5.100	15° C.	50′	745.85	48.341	15° C.	50′	1261.5	137.23	15° C.
5°	250.16	5.459	T	15°	754.32	49.441	T	25°	1270.2	139.11	T
10′	258.51	5.829	.09	10′	762.80	50.554	.19	10′	1279.0	141.01	.29
20′	266.86	6.211	E	20′	771.29	51.679	E	20′	1287.7	142.93	E
30′	275.21	6.606	.004	30′	779.77	52.818	.017	30′	1296.5	144.85	.038
40′	283.57	7.013		40′	788.26	53.969		40′	1305.3	146.79	
50′	291.92	7.432		50′	796.75	55.132		50′	1314.0	148.75	
6°	300.28	7.863		16°	805.25	56.309		26°	1322.8	150.71	
10′	308.64	8.307		10′	813.75	57.498		10′	1331.6	152.69	
20′	316.99	8.762		20′	822.25	58.699		20′	1340.4	154.69	
30′	325.35	9.230		30′	830.76	59.914		30′	1349.2	156.70	
40′	333.71	9.710	20° C.	40′	839.27	61.141	20° C.	40′	1358.0	158.72	20° C.
50′	342.08	10.202	T	50′	847.78	62.381	T	50′	1366.8	160.76	T
7°	350.44	10.707	.13	17°	856.30	63.634	.26	27°	1375.6	162.81	.39
10′	358.81	11.224	E	10′	864.82	64.900	E	10′	1384.4	164.86	E
20′	367.17	11.753	.006	20′	873.35	66.178	.022	20′	1393.2	166.95	.051
30′	375.54	12.294		30′	881.88	67.470		30′	1402.0	169.04	
40′	383.91	12.847		40′	890.41	68.774		40′	1410.9	171.15	
50′	392.28	13.413		50′	898.95	70.091		50′	1419.7	173.27	
8°	400.66	13.991		18°	907.49	71.421		28°	1428.6	175.41	
10′	409.03	14.582		10′	916.03	72.764		10′	1437.4	177.55	
20′	417.41	15.184	25° C.	20′	924.58	74.119	25° C.	20′	1446.3	179.72	25° C.
30′	425.79	15.799	T	30′	933.13	75.488	T	30′	1455.1	181.89	T
40′	434.17	16.426	.16	40′	941.69	76.869	.32	40′	1464.0	184.08	.49
50′	442.55	17.065	E	50′	950.25	78.264	E	50′	1472.9	186.29	E
9°	450.93	17.717	.007	19°	958.81	79.671	.028	29°	1481.8	188.51	.065
10′	459.32	18.381		10′	967.38	81.092		10′	1490.7	190.74	
20′	467.71	19.058		20′	975.96	82.525		20′	1499.6	192.99	
30′	476.10	19.746		30′	984.53	83.972		30′	1508.5	195.25	
40′	484.49	20.447		40′	993.12	85.431		40′	1517.4	197.53	
50′	492.88	21.161		50′	1001.7	86.904		50′	1526.3	199.82	
10°	501.28	21.887	30° C.	20°	1010.3	88.389	30° C.	30°	1535.3	202.12	30° C.
10′	509.68	22.624	T	10′	1018.9	89.888	T	10′	1544.2	204.44	T
20′	518.08	23.375	.19	20′	1027.5	91.399	.39	20′	1553.1	206.77	.59
30′	526.48	24.138	E	30′	1036.1	92.924	E	30′	1562.1	209.12	E
40′	534.89	24.913	.008	40′	1044.7	94.462	.034	40′	1571.0	211.48	.078
50′	543.29	25.700		50′	1053.3	96.013		50′	1580.0	213.86	

T = R tan ½ I E = R exsec ½ I

TABLE IX. TANGENTS AND EXTERNALS TO A 1° CURVE

I	T	E	I=40°	I	T	E	I=50°	I	T	E	I=60°
31°	1589.0	216.3	+	41°	2142.2	387.4	+	51°	2732.9	618.4	+
10′	1598.0	218.7	5° C.	10′	2151.7	390.7	5° C.	10′	2743.1	622.8	5° C.
20′	1606.9	221.1	T	20′	2161.2	394.1	T	20′	2753.4	627.2	T
30′	1615.9	223.5	.13	30′	2170.8	397.4	.17	30′	2763.7	631.7	.21
40′	1624.9	226.0	E	40′	2180.3	400.8	E	40′	2773.9	636.2	E
50′	1633.9	228.4		50′	2189.9	404.2		50′	2784.2	340.7	
32°	1643.0	230.9	.023	42°	2199.4	407.6	.037	52°	2794.5	645.2	.056
10′	1652.0	233.4		10′	2209.0	411.1		10′	2804.9	649.7	
20	1661.0	235.9		20′	2218.6	414.5		20′	2815.2	654.3	
30′	1670.0	238.4		30′	2228.1	418.0		30′	2825.6	658.8	
40′	1679.1	241.0		40′	2237.7	421.4		40′	2835.9	663.4	
50′	1688.1	243.5		50′	2247.3	425.0		50′	2846.3	668.0	
33°	1697.2	246.1	10° C.	43°	2257.0	428.5	10° C.	53°	2856.7	672.7	10° C.
10′	1706.3	248.7	T	10′	2266.6	432.0	T	10′	2867.1	677.3	T
20′	1715.3	251.3	.26	20′	2276.2	435.6	.34	20′	2877.5	682.0	.42
30′	1724.4	253.9	E	30′	2285.9	439.2	E	30′	2888.0	686.7	E
40′	1733.5	256.5	.046	40′	2295.6	442.8	.075	40′	2898.4	691.4	.112
50′	1742.6	259.1		50	2305.2	446.4		50′	2908.9	696.1	
34°	1751.7	261.8		44°	2314 9	450.0		54°	2919.4	700.9	
10′	1760.8	264.5		10′	2324.6	453.6		10′	2929.9	705.7	
20′	1770.0	267.2		20′	2334.3	457.3		20′	2940.4	710.5	
30′	1779.1	269.9		30′	2344.1	461.0		30′	2951.0	715.3	
40′	1788.2	272.6		40′	2353.8	464.6		40′	2961.5	720.1	
50′	1797.4	275.3	15° C.	50′	2363.5	468.4	15° C.	50′	2972.1	725.0	15° C.
35°	1806.6	278.1	T	45°	2373.3	472.1	T	55°	2982.7	729.9	T
10′	1815.7	280.8	.40	10′	2383.1	475.8	.51	10′	2993.3	734.8	.63
20′	1824.9	283.6	E	20′	2392.8	479.6	E	20′	3003.9	739.7	E
30′	1834.1	286.4	.070	30′	2402.6	483.4	.116	30′	3014.5	744.6	.168
40′	1843.3	289.2		40′	2412.4	487.2		40′	3025.2	749.6	
50′	1852.5	292.0		50′	2422.3	491.0		50′	3035.8	754.6	
36°	1861.7	294.9		46°	2432.1	494.8		56°	3046.5	759.6	
10′	1870.9	297.7		10′	2441.9	498.7		10′	3057.2	764.6	
20′	1880.1	300.6		20′	2451.8	502.5		20′	3067.9	769.7	
30′	1889.4	303.5		30′	2461.7	506.4		30′	3078.7	774.7	
40′	1898.6	306.4	20° C.	40′	2471.5	510.3	20° C.	40′	3089.4	779.8	20° C.
50′	1907.9	309.3	T	50′	2481.4	514.3	T	50′	3100.2	784.9	T
37°	1917.1	312.2	.53	47°	2491.3	518.2	.68	57°	3110.9	790.1	.84
10′	1926.4	315.2	E	10′	2501.2	522.2	E	10′	3121.7	795.2	E
20′	1935.7	318.1	.093	20′	2511.2	526.1	.151	20′	3132.6	800.4	.225
30′	1945.0	321.1		30′	2521.1	530.1		30′	3143.4	805.6	
40′	1954.3	324.1		40′	2531.1	534.2		40′	3154.2	810.9	
50′	1963.6	327.1		50′	2541.0	538.2		50′	3165.1	816.1	
38°	1972.9	330.2		48°	2551.0	542.2		58°	3176.0	821.4	
10′	1982.2	333.2		10′	2561.0	546.3		10′	3186.9	826.7	
20′	1991.5	336.3	25° C.	20′	2571.0	550.4	25° C.	20′	3197.8	832.0	25° C.
30′	2000.9	339.3	T	30′	2581.0	554.5	T	30′	3208.8	837.3	T
40′	2010.2	342.4	.67	40′	2591.0	558.6	.85	40′	3219.7	842.7	1.05
50′	2019.6	345.5	E	50′	2601.1	562.8	E	50′	3230.7	848.1	E
39°	2029.0	348.6	.117	49°	2611.2	566.9	.189	59°	3241.7	853.5	.283
10′	2038.4	351.8		10′	2621.2	571.1		10′	3252.7	858.9	
20′	2047.8	354.9		20′	2631.3	575.3		20′	3263.7	864.3	
30′	2057.2	358.1		30′	2641.4	579.5		30′	3274.8	869.8	
40′	2066.6	361.3		40′	2651.5	583.8		40′	3285.8	875.3	
50′	2076.0	364.5		50′	2661.6	588.0		50′	3296.9	880.8	
40°	2085.4	367.7	30° C.	50°	2671.8	592.3	30° C.	60°	3308.0	886.4	30° C.
10′	2094.9	371.0	T	10′	2681.9	596.6	T	10′	3319.1	892.0	T
20′	2104.3	374.2	.80	20′	2692.1	600.9	1.02	20′	3330.3	897.5	1.27
30′	2113.8	377.5	E	30′	2702.3	605.3	E	30′	3341.4	903.2	E
40′	2123.3	380.8	.141	40′	2712.5	609.6	.227	40′	3352.6	908.8	.340
50′	2132.7	384.1		50′	2722.7	614.0		50′	3363.8	914.5	

T = R tan ½ I E = R exsec ½ I

TABLE X.

MIDDLE ORDINATES OF RAILS

Length of Rail (feet)

C ° ′	R Feet	30 Inch	28 Inch	26 Inch	24 Inch	22 Inch	20 Inch	C °	R Feet	30 Inch	28 Inch	26 Inch	24 Inch	22 Inch	20 Inch
0–20	17189	.08	.07	.06	.05	.04	.03	8	716.8	1.88	1.64	1.42	1.20	1.01	.84
0–40	8594	.16	.14	.12	.10	.08	.07	9	637.3	2.12	1.84	1.60	1.35	1.14	.94
1–0	5730	.24	.20	.18	.15	.13	.10	10	573.7	2.36	2.05	1.78	1.50	1.27	1.04
1–20	4297	.31	.27	.23	.20	.17	.13	11	521.7	2.59	2.26	1.95	1.65	1.39	1.15
1–40	3438	.39	.34	.29	.25	.21	.17	12	478.3	3.83	2.47	2.15	1.81	1.54	1.26
2–0	2865	.47	.41	.35	.30	.25	.20	13	441.7	3.05	2.66	2.30	1.96	1.66	1.36
2–20	2456	.55	.48	.41	.35	.29	.23	14	410.3	3.30	2.87	2.48	2.10	1.78	1.46
2–40	2149	.63	.55	.47	.40	.33	.27	15	383.1	3.54	3.08	2.68	2.26	1.91	1.57
3–0	1910	.71	.62	.53	.45	.38	.31	16	359.3	3.76	3.28	2.83	2.40	2.04	1.67
3–20	1719	.78	.68	.59	.50	.42	.35	17	338.3	4.00	3.48	3.02	2.57	2.16	1.78
3–40	1563	.86	.75	.65	.55	.46	.38	18	319.6	4.21	3.67	3.18	2.70	2.28	1.87
4–0	1433	.94	.82	.71	.60	.50	.42	19	302.9	4.45	3.89	3.36	2.86	2.41	1.98
4–20	1323	1.02	.89	.77	.65	.55	.45	20	287.9	4.70	4.09	3.55	3.00	2.54	2.09
4–40	1228	1.10	.96	.83	.70	.59	.48	22	262.0	5.16	4.44	3.84	3.30	2.80	2.29
5	1146	1.18	1.03	.89	.75	.63	.52	24	240.5	5.64	4.92	4.20	3.59	3.04	2.50
6	955.3	1.41	1.23	1.06	.90	.76	.62	26	222.3	6.07	5.29	4.58	3.88	3.29	2.70
7	819.0	1.65	1.44	1.24	1.05	.89	.73								

TABLE XI.

SHORT RADIUS CURVES

Radius Feet	Chord Feet	Central Angle	Deflection Angle	Deflection for 1 Foot
35	10	16-26	8-13	49.3
45	10	12-46	6-23	38.3
50	15	17-16	8-38	34.5
60	15	14-22	7-11	28.8
75	15	11-30	5-45	23.0
100	20	11-30	5-45	17.3
120	20	9-34	4-47	14.3
150	20	7-39	3-49	11.5
190	25	7-32	3-46	9.15
200	25	7-10	3-35	8.6
225	25	6-25	3-12	7.7
240	25	5-58	2-59	7.2
250	25	5-44	2-52	6.9
275	25	5-12	2-36	6.2
288	50	9-58	4-59	6.0
300	50	9-32	4-46	5.7
350	50	8-12	4-06	4.9
376	50	7-40	3-50	4.6
400	50	7-10	3-35	4.3
410	50	7-00	3-30	4.2

To find length of curve divide angle from P. C. to P. T. by central angle of chord and multiply by length of chord.

TABLE XII.

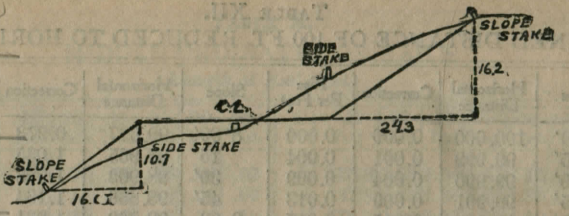
INCLINED DISTANCE OF 100 FT. REDUCED TO HORIZONTAL

Slope	Horizontal Distance	Correction	Rise Per Foot	Slope	Horizontal Distance	Correction	Rise Per Foot
0°00′	100.000	0.000	0.000	8°00′	99.027	0.973	0.139
15′	99.999	0.001	0.004	15′	98.965	1.035	0.143
30′	99.996	0.004	0.009	30′	98.902	1.098	0.148
45′	99.991	0.009	0.013	45′	98.836	1.164	0.152
1 00	99.985	0.015	0.017	9 00	98.769	1.231	0.156
15	99.976	0.024	0.022	15	98.700	1.300	0.161
30	99.966	0.034	0.026	30	98.629	1.371	0.165
45	99.953	0.047	0.031	45	98.556	1.444	0.169
2 00	99.939	0.061	0.035	10 00	98.481	1.519	0.174
15	99.923	0.077	0.039	15	98.404	1.596	0.178
30	99.905	0.095	0.044	30	98.325	1.675	0.182
45	99.885	0.115	0.048	45	98.245	1.755	0.187
3 00	99.863	0.137	0.052	11 00	98.163	1.837	0.191
15	99.839	0.161	0.057	15	98.079	1.921	0.195
30	99.813	0.187	0.061	30	97.992	2.008	0.199
45	99.786	0.214	0.065	45	97.905	2.095	0.204
4 00	99.756	0.244	0.070	12 00	97.815	2.185	0.208
15	99.725	0.275	0.074	15	97.723	2.277	0.212
30	99.692	0.308	0.078	30	97.630	2.370	0.216
45	99.657	0.343	0.083	45	97.534	2.466	0.221
5 00	99.619	0.381	0.087	13 00	97.437	2.563	0.225
15	99.580	0.420	0.092	15	97.338	2.662	0.229
30	99.540	0.460	0.096	30	97.237	2.763	0.233
45	99.497	0.503	0.100	45	97.134	2.866	0.238
6 00	99.452	0.548	0.105	14 00	97.030	2.970	0.242
15	99.406	0.594	0.109	15	96.923	3.077	0.246
30	99.357	0.643	0.113	30	96.815	3.185	0.250
45	99.307	0.693	0.118	45	96.705	3.295	0.255
7 00	99.255	0.745	0.122	15 00	96.593	3.407	0.259
15	99.200	0.800	0.126	15	96.479	3.521	0.263
30	99.144	0.856	0.131	30	96.363	3.637	0.267
45	99.087	0.913	0.135	45	96.246	3.754	0.271

TABLE XIII.

MINUTES IN DECIMALS OF A DEGREE.

0 30″	.00833	10′ 30″	.17500	20′ 30″	.34167	30′ 10″	.50833	40′ 30″	.67500	50′ 10″	.84167
1 00	.01667	11 00	.18333	21 00	.35000	31 00	.51667	41 00	.68333	51 00	.85000
30	.02500	30	.19167	30	.35833	30	.52500	30	.69167	30	.85833
2 00	.03333	12 00	.20000	22 00	.36667	32 00	.53333	42 00	.70000	52 00	.86667
30	.04167	30	.20833	30	.37500	30	.54167	30	.70833	30	.87500
3 00	.05000	13 00	.21667	23 00	.38333	33 00	.55000	43 00	.71667	53 00	.88333
30	.05833	30	.22500	30	.39167	30	.55833	30	.72500	30	.89167
4 00	.06667	14 00	.23333	24 00	.40000	34 00	.56667	44 00	.73333	54 00	.90000
30	.07500	30	.24167	30	.40833	30	.57500	30	.74167	30	.90833
5 00	.08333	15 00	.25000	25 00	.41667	35 00	.58333	45 00	.75000	55 00	.91667
30	.09167	30	.25833	30	.42500	30	.59167	30	.75833	30	.92500
6 00	.10000	16 00	.26667	26 00	.43333	36 00	.60000	46 00	.76667	56 00	.93333
30	.10833	30	.27500	30	.44167	30	.60833	30	.77500	30	.94167
7 00	.11667	17 00	.28333	27 00	.45000	37 00	.61667	47 00	.78333	57 00	.95000
30	.12500	30	.29167	30	.45833	30	.62500	30	.79167	30	.95833
8 00	.13333	18 00	.30000	28 00	.46667	38 00	.63333	48 00	.80000	58 00	.96667
30	.14167	30	.30833	30	.47500	30	.64167	30	.80833	30	.97500
9 00	.15000	19 00	.31667	29 00	.48333	39 00	.65000	49 00	.81667	59 00	.98333
30	.15833	30	.32500	30	.49167	30	.65833	30	.82500	30	.99167
10 00	.16667	20 00	.33333	30 00	.50000	40 00	.66667	50 00	.83333	60 00	1.00000



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1 65	1 80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3 45	3.60	3 75	3.90	4.05	4.20	4 35	2
3	4.50	4 65	4.80	4.95	5 10	5 25	5 40	5.55	5.70	5.85	3
4	6.00	6 15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7 50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9 00	9 15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10 65	10.80	10.95	11.10	11.25	11.40	11.55	11 70	11.85	7
8	12.00	12 15	12.30	12.45	12.60	12.75	12.90	13 05	13.20	13.35	8
9	13 50	13.65	13 80	13 95	14.10	14.25	14.40	14 55	14.70	14.85	9
10	15.00	15 15	15 30	15 45	15.60	15.75	15.90	16.05	16.20	16 35	10
11	16 50	16 65	16 80	16.95	17 10	17.25	17.40	17.55	17.70	17.85	11
12	18 00	18 15	18.30	18 45	18.60	18 75	18.90	19.05	19.20	19 35	12
13	19 50	19 65	19.80	19.95	20.10	20.25	20 40	20.55	20.70	20.85	13
14	21.00	21 15	21.30	21.45	21 60	21.75	21.90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24 15	24 30	24 45	24 60	24.75	24 90	25 05	25.20	25.35	16
17	25.50	25 65	25.80	25 95	26.10	26 25	26 40	26.55	26.70	26.85	17
18	27.00	27 15	27.30	27 45	27.60	27.75	27.90	28.05	28 20	28.35	18
19	28 50	28 65	28 80	28.95	29.10	29.25	29 40	29.55	29.70	29.85	19
20	30 00	30 15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31 50	31 65	31.80	31.95	32 10	32 25	32.40	32.55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33.60	33 75	33.90	34.05	34.20	34.35	22
23	34 50	34 65	34.80	34.95	35.10	35 25	35 40	35.55	35.70	35 85	23
24	36.00	36 15	36.30	36 45	36.60	36.75	36.90	37.05	37 20	37.35	24
25	37.50	37.65	37 80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39 00	39 15	39.30	39 45	39 60	39.75	39.90	40.05	40.20	40.35	26
27	40 50	40 65	40 80	40.95	41.10	41.25	41 40	41.55	41.70	41.85	27
28	42 00	42 15	42.30	42.45	42.60	42 75	42.90	43.05	43.20	43.35	28
29	43 50	43 65	43.80	43 95	44.10	44 25	44 40	44.55	44.70	44 85	29
30	45 00	45 15	45.30	45 45	45.60	45.75	45.90	46.05	46 20	46.35	30
31	46.50	46.65	46.80	46 95	47.10	47 25	47.40	47.55	47.70	47.85	31
32	48 00	48.15	48.30	48 45	48.60	48 75	48.90	49.05	49 20	49.35	32
33	49.50	49 65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51 00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52 50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54 00	54 15	54.30	54 45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55 50	55 65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57 45	57.60	57 75	57.90	58.05	58.20	58 35	38
39	58 50	58.65	58 80	58.95	59.10	59 25	59.40	59 55	59.70	59.85	39
40	60 00	60 15	60 30	60 45	60 60	60.75	60 90	61.05	61 20	61.35	40
41	61.50	61 65	61 80	61 95	62 10	62 25	62.40	62 55	62 70	62.85	41
42	63 00	63.15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64.35	42
43	64.50	64 65	64 80	64.95	65.10	65 25	65 40	65.55	65.70	65.85	43
44	66 00	66 15	66 30	66.45	66.60	66 75	66.90	67.05	67.20	67.35	44
45	67 50	67 65	67 80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69 00	69 15	69 30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70 50	70 65	70 80	70 95	71.10	71.25	71 40	71.55	71.70	71.85	47
48	72.00	72 15	72.30	72.45	72.60	72.75	72.90	73 05	73.20	73 35	48
49	73 50	73 65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

Computed by L. Leland Locke.